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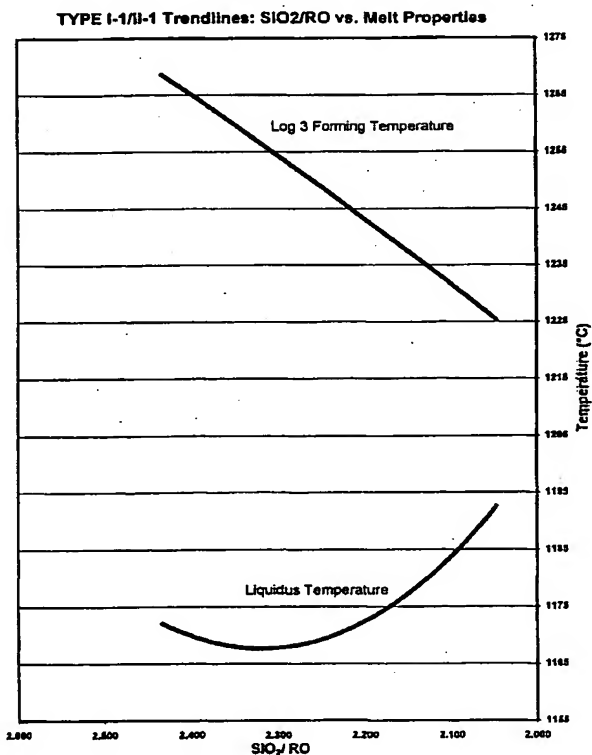
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(54) Title: GLASS FIBER FORMING COMPOSITIONS



(57) Abstract: A glass fiber composition has 52 to 62 percent by weight SiO<sub>2</sub>, 0 to 2 percent by weight Na<sub>2</sub>O, 16 to 25 percent by weight CaO, 8 to 16 percent by weight Al<sub>2</sub>O<sub>3</sub>, 0.05 to 0.80 percent by weight Fe<sub>2</sub>O<sub>3</sub>, 0 to 2 percent by weight K<sub>2</sub>O, 1 to 5 percent by weight MgO, 0 to 5 percent by weight B<sub>2</sub>O<sub>3</sub>, to 0 to 2 percent by weight TiO<sub>2</sub>, and 0 to 1 percent by weight F, and further has a log 3 forming temperature of no greater than 1240 °C based on an NIST 714 reference standard, a ΔT of at least 50 °C, and a SiO<sub>2</sub>/RO ratio of no greater than 2.35.

WO 02/20419 A1



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## **GLASS FIBER FORMING COMPOSITIONS**

### **Cross Reference to Related Patent Applications**

This application claims the benefit of U.S. Provisional Application No.  
5 60/230474, filed September 6, 2000 and PCT Application No. US 00/14155, filed  
May 23, 2000.

The present invention relates to glass compositions for making glass fibers,  
and more particular to glass compositions having lowered liquidus and forming  
10 temperatures.

The most common glass composition for making continuous glass fiber  
strands for textiles and glass fiber reinforcements is "E" glass. The requirements as  
to what type of composition constitutes an E-glass composition are included in ASTM  
D578-98. An advantage of using E-glass is that its liquidus temperature is well  
15 below its forming temperature, i.e. typically greater than 56°C (100°F) and generally  
between 83 to 111°C (150 to 200°F). As used herein, the terms "forming  
temperature", " $T_{\text{FORM}}$ " and "log 3 forming temperature" mean the temperature of the  
glass at which the viscosity of the glass is log 3, or 1000 poise, and the terms  
"liquidus temperature" and " $T_{\text{LIQ}}$ " mean the temperature at which solid phase  
20 (crystals) and liquid phase (melt) are in equilibrium. The difference between  $T_{\text{FORM}}$   
and  $T_{\text{LIQ}}$ , referred to herein as "delta T" or " $\Delta T$ ", is a common measure of the  
crystallization potential of a given melt composition. In the glass fiber forming  
industry,  $\Delta T$  is typically maintained at a temperature of at least 50°C (90°F) in order  
to prevent devitrification of the molten glass during a glass fiber forming operation,  
25 and in particular in the bushing area.

Boron and fluorine containing glass were developed to meet these operating  
conditions. More specifically, the boron and fluorine were included in the glass batch  
materials to act as fluxes during the glass melting operation. In particular, E-glass  
can include up to 10 wt%  $\text{B}_2\text{O}_3$  and up to 1.0 fluoride (see ASTM D 578-00 §4.2).  
30 However, these materials are volatilized during melting and boron and fluorine  
emissions are released to the atmosphere. Since boron and fluorine are considered  
pollutants, these emissions are closely controlled by environmental regulations,  
which in turn requires careful control of the furnace operations and the use of

- 2 -

expensive pollution control equipment. In response to this, low boron and/or low fluorine E-glasses were developed. As used herein, "low boron" means that the glass composition is no greater than 5 weight percent (wt%) boron, and includes boron-free glass, and "low fluorine" means that the glass composition is no greater than 0.30 wt% fluorine, and includes fluorine-free glass.

For additional information concerning glass compositions and methods for fiberizing the glass composition, see K. Loewenstein, The Manufacturing Technology of Continuous Glass Fibres, (3d Ed. 1993) at pages 30-44, 47-60, 115-122 and 126-135, and F. T. Wallenberger (editor), Advanced Inorganic Fibers: Processes, Structures, Properties, Applications, (2000) at pages 81-102 and 129-168, which are hereby incorporated by reference.

Because the actual glass fiber forming operation is conducted at high temperatures, there is high energy usage associated with its production, along with associated high energy costs. In addition, the high temperatures accelerate the degradation of the refractory used in the glass melting furnace, as well as the bushings used to form the fibers. The bushings include precious metals that cannot be recovered from the glass as the bushings corrode. It would be advantageous to produce the glass fibers at the lowest possible forming and liquidus temperatures so as to reduce the energy usage and costs and thermal load on the furnace refractory and bushings, while at the same time provide the  $\Delta T$  required to ensure an uninterrupted glass fiber forming operation. Reducing the forming and liquidus temperatures of the glass compositions can also result in environmental benefits, such as but not limited to, a reduction in the amount of fuel required to generate the energy necessary for the fiber forming operation, as well as a reduction in the flue gas temperature. In addition, it would be advantageous if the glass compositions are low fluorine and/or low boron compositions so as to reduce or eliminate the environmental pollutants associated with these materials.

The present invention provides a low boron content glass fiber forming composition that has a forming temperature of no greater than 1240°C (2262°F), a  $\Delta T$  of at least 50°C (90°F), and a ratio of  $\text{SiO}_2$  to RO (i.e.  $\text{CaO} + \text{MgO}$ ) of no greater than 2.35. In one nonlimiting embodiment of the present invention, the glass composition has a silica content of no greater than 59 weight percent. In another nonlimiting embodiment of the invention, the glass composition is boron-free.

- 3 -

The foregoing summary, as well as the following detailed description of embodiments of the present invention, will be better understood when read in conjunction with the appended drawings. In the drawings:

Figures 1-6 are curves showing the relationship between the ratio of SiO<sub>2</sub> to RO of various glass fiber forming compositions to the compositions' forming and liquidus temperatures based on the data shown in corresponding Tables A through F, respectively.

The base composition for the low boron glass fibers of the present invention suitable for textiles and glass fiber reinforcements includes the following main constituents in weight percent based on the total weight of the final glass composition.

	<u>broad range</u>	<u>alternate range</u>
SiO <sub>2</sub> (wt%)	52 to 62	53 to 59
Na <sub>2</sub> O (wt%)	0 to 2	up to 1.5
CaO (wt%)	16 to 25	20 to 25
Al <sub>2</sub> O <sub>3</sub> (wt%)	8 to 16	11 to 14
Fe <sub>2</sub> O <sub>3</sub> (wt%)	0.05 to 0.80	up to 0.5
K <sub>2</sub> O (wt%)	0 to 2	up to 1

It should be appreciated that, unless otherwise indicated, all numerical values discussed herein, such as but not limited to weight percent of materials or temperatures, are approximate and are subject to variations due to various factors well known to those skilled in the art such as, but not limited to, measurement standards, equipment and techniques. As a result, such values are to be understood as being modified in all instances by the term "about". Accordingly, unless indicated to the contrary, the numerical parameters set forth in the following specification and attached claims are approximations that may vary depending upon the desired properties sought to be obtained by the present invention. At the very least, each numerical parameter should at least be construed in light of the number of reported significant digits and by applying ordinary rounding techniques. For example, where it states in the present application that the range for SiO<sub>2</sub> is 52 to 62 weight percent, this range is about 52 to about 62 weight percent, and where it states that the forming temperature of a glass composition should be no greater than 1249°C (2280°F), the temperature is about 1249°C.

- 4 -

Notwithstanding that the numerical ranges and parameters setting forth the broad scope of the invention are approximations, the numerical values set forth in the specific examples are reported as precisely as possible. Any numerical value, however, inherently contain certain errors necessarily resulting from the standard deviation found in their respective testing measurements.

In addition, where the amount of a particular material or combinations of materials disclosed herein is expressed in terms of "percent" or "%", it should be understood that this means "weight percent" or "wt%".

Additional materials can be added to the glass composition to modify the melt properties of the glass. For example, and without limiting the glass compositions disclosed herein,  $\text{Li}_2\text{O}$ ,  $\text{ZnO}$ ,  $\text{MnO}$  and/or  $\text{MnO}_2$ , can be added to the glass fiber composition to reduce  $T_{\text{FORM}}$  and/or  $T_{\text{LIQ}}$ . In one non-limiting embodiment of the present invention, the glass composition includes 0 to 1.5 wt%  $\text{Li}_2\text{O}$  and/or 0 to 1.5 wt%  $\text{ZnO}$  and/or 0 to 3 wt%  $\text{MnO}$  and/or 0 to 3 wt%  $\text{MnO}_2$ . It is believed that levels of these materials less than 0.05 wt% would be considered either tramp amounts or so low that they will not materially impact the glass melt properties. As a result, in another non-limiting embodiment, 0.05 to 1.5 wt%  $\text{Li}_2\text{O}$  and/or 0.05 to 1.5 wt%  $\text{ZnO}$  and/or 0.05 to 3 wt%  $\text{MnO}$  and/or 0.05 to 3 wt%  $\text{MnO}_2$  are included in the glass composition. In still another nonlimiting embodiment of the invention, the glass compositions include 0.2 to 1 wt%  $\text{Li}_2\text{O}$  and/or 0.2 to 1 wt%  $\text{ZnO}$  and/or up to 1 wt%  $\text{MnO}$  and/or up to 1 wt%  $\text{MnO}_2$ .

$\text{MgO}$  is another material typically included in a glass fiber forming composition. It has been found that the heating and melting profile of a glass fiber composition, and in particular the liquidus temperature, can be controlled and in particular optimized by controlling the amount of  $\text{MgO}$ . In addition, it has been determined that a eutectic (minimum liquidus temperature) exists in a generic quaternary  $\text{SiO}_2\text{-Al}_2\text{O}_3\text{-CaO-MgO}$  at around 2.5 wt%  $\text{MgO}$  (see PCT Application No. US 00/14155, which is incorporated herein by reference). Without limiting the present invention, in one nonlimiting embodiment, the glass fiber composition includes 1 to 5 wt%  $\text{MgO}$ , e.g. 1 to 4 wt% or 1.7 to 2.9 wt% or 1.9 to 2.65 wt%  $\text{MgO}$ .

Boron is another material that can be added to glass fiber compositions to reduce  $T_{\text{FORM}}$  and  $T_{\text{LIQ}}$ . However, as discussed earlier, the inclusion of boron results in the production of particulate emissions that, depending on the particulate level,

- 5 -

may have to be removed from a melting furnace exhaust stream before being released into the environment. Although the amount of  $B_2O_3$  in a glass fiber composition can be as high as 10 wt%, in the present invention, the glass composition has a low boron content, i.e. has a  $B_2O_3$  content of no greater than 5 wt%. In other nonlimiting embodiments of the present invention, the glass fiber composition has no greater than 4 wt%, or no greater than 3 wt%, or no greater than 2 wt%  $B_2O_3$ . In another nonlimiting embodiment of a glass fiber forming composition, the low boron content glass composition is essentially boron-free, i.e. it includes no more than a trace amount of  $B_2O_3$ , which is considered herein to be up to 0.05 wt%  $B_2O_3$ . In still another nonlimiting embodiment, the low boron content glass fiber composition does not include any  $B_2O_3$ .

It should be appreciated that glass fiber compositions can include other constituents and the present invention contemplates the inclusion of other materials in the glass fiber compositions, such as, but not limited to, 0 to 2 wt% each of  $TiO_2$ ,  $BaO$ ,  $ZrO_2$  and  $SrO$ , e.g. up to 1.5 wt% or up to 1 wt% of each of these materials.

In addition, because of the environmental concerns discussed earlier, in one nonlimiting embodiment of the present invention, the glass composition has a low fluorine content. In another nonlimiting embodiment, the glass composition is fluorine-free, i.e. it includes no more than a trace amount of fluorine, which is considered herein to be up to 0.05 wt% fluorine. In still another nonlimiting embodiment, the glass composition does not include any fluorine. Except where otherwise indicated, the glass fiber forming compositions disclosed and discussed herein are fluorine-free.

It should be appreciated that the glass compositions disclosed herein can also include small amounts of other materials, for example melting and refining aids, tramp materials or impurities. For example and without limiting the present invention, melting and refining aids, such as  $SO_3$ , are useful during production of the glass, but their residual amounts in the glass can vary and have minimal, if any, material effect on the properties of the glass product. In addition, small amounts of the additives discussed above can enter the glass composition as tramp materials or impurities included in the raw materials of the main constituents.

Commercial glass fibers of the present invention can be prepared in the conventional manner well known in the art, by blending the raw materials used to

- 6 -

supply the specific oxides that form the composition of the fibers. For example, typically sand is used for  $\text{SiO}_2$ , clay for  $\text{Al}_2\text{O}_3$ , lime or limestone for  $\text{CaO}$ , and dolomite for  $\text{MgO}$  and some of the  $\text{CaO}$ . As discussed earlier, the glass can include other additives that are added to modify the glass properties as well as small amounts of melting and refining aids, tramp materials or impurities.

After the ingredients are mixed in the proper proportions to provide the desired weight of each constituent for the desired glass, the batch is melted in a conventional glass fiber melting furnace and the resulting molten glass is passed along a conventional forehearth and into a glass fiber forming bushing located along the bottom of the forehearth, as is well known to those skilled in the art. During the glass melting phase, the glass batch materials are typically heated to a temperature of at least  $1400^\circ\text{C}$  ( $2550^\circ\text{F}$ ). The molten glass is then drawn or pulled through a plurality of holes in the bottom of the bushing. The streams of molten glass are attenuated to form filaments by gathering a plurality of filaments together to form a strand and winding the strand on a forming tube mounted on a rotatable collet of a winding machine. Alternatively, the fiber forming apparatus can be, for example, a forming device for synthetic textile fibers or strands in which fibers are drawn from nozzles, for example a spinneret, wherein fibers are drawn through holes in a plate, as is known to those skilled in the art. Typical forehearths and glass fiber forming arrangements are shown in K. Loewenstein, The Manufacturing Technology of Continuous Glass Fibres, (Third Edition 1993) at pages 85-107 and pages 115-135, which are hereby incorporated by reference.

Several series of different types of low boron glass fiber compositions were made to examine certain relationships between the amount of selected glass constituents and the corresponding forming and liquidus temperatures in order to identify glass compositions having a lowered forming temperature and a desired  $\Delta T$ . During testing, the glass compositions for the different series of experimental samples were divided into the following main compositional categories and subcategories:



- 7 -

Type I – high  $T_{\text{FORM}}$  ( $T_{\text{FORM}} > 1240^{\circ}\text{C}$ ), low boron content

Type I-1 boron-free

Type I-2 up to 2.5 wt%  $\text{B}_2\text{O}_3$

Type II - low  $T_{\text{FORM}}$  ( $T_{\text{FORM}} \leq 1240^{\circ}\text{C}$ ), low boron content, 2.5 wt% MgO

Type II-1 boron-free

Type II-2 up to 5 wt%  $\text{B}_2\text{O}_3$

Type III - low  $T_{\text{FORM}}$  ( $T_{\text{FORM}} \leq 1240^{\circ}\text{C}$ ), low boron content, 2.5 wt% MgO,  
lithium and/or zinc

Type III-1 boron-free with lithium

Type III-2 boron-free with lithium and zinc

Type III-3 boron-free with zinc

Type III-4 up to 5 wt%  $\text{B}_2\text{O}_3$  with lithium

Type I-1 glasses would include prior art glasses such as those disclosed in Example 1 of French Patent 2,768,144 (hereinafter "Patent '144"), U.S. Patents 4,542,106 and 5,789,329 (hereinafter "Patent '106" and "Patent '329", respectively), and ADVANTEX® glass, which is commercially available from Owens Corning Fiberglass, and typically include approximately 60 wt%  $\text{SiO}_2$ , 25 wt%  $\text{CaO} + \text{MgO}$  (hereinafter "RO"), and 12-14 wt%  $\text{Al}_2\text{O}_3$  and are boron-free. Type I-2 glasses would include prior art glasses such as that disclosed in Example 2 Patent '144, which includes 1.8 wt%  $\text{B}_2\text{O}_3$  and 60.82 wt%  $\text{SiO}_2$ .

Tables A through F include examples of each series of glass fiber compositions and were used to generate corresponding Figures 1-6, respectively, as will be discussed later in more detail. In Table A, Examples 1-8 are Type II-1 glasses while Examples 9-34 are Type I-1 glasses. In Table B, Examples 35-77 are Type II-2 glasses while Examples 78-83 are Type I-2 glasses. In Table C, Examples 84-143 and 152-156 are Type III-1 glasses while Examples 144-151 are similar but have a log 3 forming temperature greater than  $1240^{\circ}\text{C}$ . In Table D, Examples 157-171 are Type III-2 glasses while Examples 172-183 are similar but have a log 3 forming temperature greater than  $1240^{\circ}\text{C}$ . In Table E, Examples 194-197 are Type III-3 glasses while Examples 184-193 are similar but have a log 3 forming temperature greater than  $1240^{\circ}\text{C}$ . In Table F, Examples 198-296 are Type III-4 glasses while Examples 297 and 298 are similar but have a log 3 forming temperature greater than  $1240^{\circ}\text{C}$ .

TABLE A – TYPE I-1 AND II-1 GLASS

Composition Weight %	Examples									
	1	2	3	4	5	6	7	8	9	10
SiO <sub>2</sub>	57.95	57.75	58.05	57.65	57.45	58.72	57.72	59.05	60.13	60.63
Al <sub>2</sub> O <sub>3</sub>	13.20	13.20	13.40	13.40	13.40	11.65	11.64	12.20	12.27	12.27
CaO	24.05	24.25	23.75	24.15	24.35	24.58	25.58	23.95	22.92	22.42
MgO	2.55	2.55	2.55	2.55	2.55	2.61	2.61	2.55	2.50	2.50
TiO <sub>2</sub>	1.10	1.10	1.10	1.10	1.10	1.12	1.12	1.10	1.00	1.00
Na <sub>2</sub> O	0.90	0.90	0.90	0.90	0.90	0.92	0.92	0.90		0.98
K <sub>2</sub> O						0.05	0.05			
Fe <sub>2</sub> O <sub>3</sub>	0.25	0.25	0.25	0.25	0.25	0.27	0.27	0.25	0.20	0.20
SO <sub>3</sub>						0.02	0.02			
SiO <sub>2</sub> /RO	2.18	2.15	2.21	2.16	2.13	2.16	2.05	2.23	2.37	2.43
T <sub>FORM</sub> (°C)	1235	1232	1240	1240	1238	1230	1222	1239	1265	1268
T <sub>LIQ</sub> (°C)	1164	1166	1167	1166	1165	1198	1215	1181	1164	1166
ΔT (°C)	71	66	73	74	74	32	7	58	101	102

5

TABLE A – TYPE I-1 AND II-1 GLASS (cont'd)

Composition Weight %	Examples									
	11	12	13	14	15	16	17	18	19	20
SiO <sub>2</sub>	60.13	59.61	59.45	59.40	59.35	59.30	59.25	59.10	59.00	58.85
Al <sub>2</sub> O <sub>3</sub>	12.27	12.16	12.20	12.20	12.20	12.20	12.20	12.20	12.20	12.20
CaO	22.92	23.51	23.55	23.60	23.65	23.70	23.75	23.90	24.00	24.15
MgO	2.50	2.62	2.55	2.55	2.55	2.55	2.55	2.55	2.55	2.55
TiO <sub>2</sub>	1.00	1.00	1.10	1.10	1.10	1.10	1.10	1.10	1.10	1.10
Na <sub>2</sub> O	0.98	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
K <sub>2</sub> O										
Fe <sub>2</sub> O <sub>3</sub>	0.20	0.20	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25
SO <sub>3</sub>										
SiO <sub>2</sub> /RO	2.37	2.28	2.28	2.27	2.27	2.26	2.25	2.23	2.22	2.20
T <sub>FORM</sub> (°C)	1262	1251	1258	1250	1242	1248	1249	1247	1245	1242
T <sub>LIQ</sub> (°C)	1164	1170	1173	1178	1176	1180	1178	1178	1178	1186
ΔT (°C)	98	81	85	72	66	68	71	69	67	56

TABLE A – TYPE I-1 AND II-1 GLASS (cont'd)

Composition Weight %	Examples									
	21	22	23	24	25	26	27	28	29	30
SiO <sub>2</sub>	59.25	59.15	58.35	58.15	58.25	57.85	57.65	58.15	57.95	57.75
Al <sub>2</sub> O <sub>3</sub>	12.40	12.60	13.20	13.20	13.40	13.40	13.40	13.20	13.20	13.20
CaO	23.55	23.45	23.65	23.85	23.55	23.95	24.15	23.85	24.05	24.25
MgO	2.55	2.55	2.55	2.55	2.55	2.55	2.55	2.55	2.55	2.55
TiO <sub>2</sub>	1.10	1.10	1.10	1.10	1.10	1.10	1.10	1.10	1.10	1.10
Na <sub>2</sub> O	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
K <sub>2</sub> O										
Fe <sub>2</sub> O <sub>3</sub>	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25
SO <sub>3</sub>										
SiO <sub>2</sub> /RO	2.27	2.28	2.23	2.20	2.23	2.18	2.16	2.20	2.18	2.15
T <sub>FORM</sub> (°C)	1253	1253	1248	1245	1244	1243	1242	1249	1246	1243
T <sub>LIQ</sub> (°C)	1171	1168	1162	1160	1174	1174	1169	1170	1171	1172
ΔT (°C)	82	85	86	85	70	69	73	79	75	71

TABLE A – TYPE I-1 AND II-1 GLASS (cont'd)

Composition Weight %	Examples			
	31	32	33	34
SiO <sub>2</sub>	57.55	58.05	58.85	59.61
Al <sub>2</sub> O <sub>3</sub>	13.20	13.40	13.40	12.16
CaO	24.45	23.75	23.95	23.51
MgO	2.55	2.55	2.55	2.62
TiO <sub>2</sub>	1.10	1.10	1.10	1.00
Na <sub>2</sub> O	0.90	0.90	0.90	0.90
K <sub>2</sub> O				
Fe <sub>2</sub> O <sub>3</sub>	0.25	0.25	0.25	0.20
SO <sub>3</sub>				
SiO <sub>2</sub> /RO	2.13	2.21	2.22	2.28
T <sub>FORM</sub> (°C)	1241	1246	1248	1251
T <sub>LIQ</sub> (°C)	1164	1163	1171	1167
ΔT (°C)	67	83	77	84

- 10 -

TABLE B – TYPE I-2 AND II-2 GLASS

Composition Weight %	Examples									
	35	36	37	38	39	40	41	42	43	44
SiO <sub>2</sub>	57.75	57.75	56.75	57.15	57.25	58.55	55.40	55.80	56.20	55.75
Al <sub>2</sub> O <sub>3</sub>	13.20	12.20	13.20	13.05	13.20	12.20	13.60	13.40	13.60	13.20
CaO	24.25	24.25	24.25	24.00	24.25	23.45	24.85	24.65	24.05	23.25
MgO	2.50	2.50	2.50	2.55	2.50	2.55	2.50	2.50	2.50	2.55
TiO <sub>2</sub>	1.10	1.10	1.10	1.10	1.10	1.10	0.50	0.50	0.50	1.10
Na <sub>2</sub> O	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Fe <sub>2</sub> O <sub>3</sub>	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25
B <sub>2</sub> O <sub>3</sub>	1.00	1.00	1.00	1.00	1.00	1.00	2.00	2.00	2.00	3.00
SiO <sub>2</sub> /RO	2.16	2.16	2.12	2.15	2.14	2.25	2.03	2.06	2.12	2.16
T <sub>FORM</sub> (°C)	1240	1227	1228	1235	1239	1236	1217	1211	1219	1204
T <sub>LIQ</sub> (°C)	1178	1164	1161	1154	1159	1159	1153	1156	1136	1127
ΔT (°C)	62	63	67	81	80	77	64	55	83	77

TABLE B – TYPE I-2 AND II-2 GLASS (cont'd)

Composition Weight %	Examples									
	45	46	47	48	49	50	51	52	53	54
SiO <sub>2</sub>	57.25	56.25	56.65	56.75	58.05	56.35	56.40	56.45	55.60	55.80
Al <sub>2</sub> O <sub>3</sub>	12.20	13.20	13.05	13.20	12.20	13.60	13.60	13.55	13.60	13.60
CaO	23.75	23.75	23.50	23.25	22.95	23.85	23.80	23.80	24.65	24.45
MgO	2.50	2.50	2.55	2.55	2.55	2.55	2.55	2.55	2.50	2.50
TiO <sub>2</sub>	1.10	1.10	1.10	1.10	1.10	0.50	0.50	0.50	0.50	0.50
Na <sub>2</sub> O	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Fe <sub>2</sub> O <sub>3</sub>	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25
B <sub>2</sub> O <sub>3</sub>	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
SiO <sub>2</sub> /RO	2.18	2.14	2.17	2.20	2.28	2.13	2.14	2.14	2.05	2.07
T <sub>FORM</sub> (°C)	1227	1224	1225	1225	1225	1218	1219	1220	1211	1209
T <sub>LIQ</sub> (°C)	1148	1149	1145	1147	1142	1138	1142	1137	1154	1156
ΔT (°C)	79	75	80	78	83	80	77	83	57	53

- 11 -

TABLE B – TYPE I-2 AND II-2 GLASS (cont'd)

Composition Weight %	Examples									
	55	56	57	58	59	60	61	62	63	64
SiO <sub>2</sub>	56.50	56.60	56.40	56.0	56.40	56.20	56.00	56.00	55.80	56.50
Al <sub>2</sub> O <sub>3</sub>	13.55	13.40	13.40	13.60	13.60	13.80	13.80	13.60	13.60	13.20
CaO	23.85	23.85	24.05	24.25	23.85	23.85	24.05	24.25	24.45	23.50
MgO	2.55	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.55
TiO <sub>2</sub>	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	1.10
Na <sub>2</sub> O	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.9	0.90
Fe <sub>2</sub> O <sub>3</sub>	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25
B <sub>2</sub> O <sub>3</sub>	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
SiO <sub>2</sub> /RO	2.14	2.15	2.12	2.09	2.14	2.13	2.11	2.09	2.07	2.16
T <sub>FORM</sub> (°C)	1217	1222	1216	1213	1220	1223	1219	1202	1222	1220
T <sub>LIQ</sub> (°C)	1135	1139	1143	1136	1139	1158	1151	1137	1153	1133
ΔT (°C)	82	83	73	77	81	65	68	65	69	87

TABLE B – TYPE I-2 AND II-2 GLASS (cont'd)

Composition Weight %	Examples									
	65	66	67	68	69	70	71	72	73	74
SiO <sub>2</sub>	57.25	56.75	56.25	56.75	56.65	56.80	56.40	55.80	55.60	55.00
Al <sub>2</sub> O <sub>3</sub>	13.20	13.20	13.20	13.45	13.05	13.40	13.80	13.80	13.40	13.80
CaO	22.75	23.75	23.75	23.00	23.50	23.65	23.65	24.25	24.85	25.05
MgO	2.50	2.05	2.55	2.55	2.55	2.50	2.50	2.50	2.50	2.50
TiO <sub>2</sub>	1.10	1.10	1.10	1.10	1.10	0.50	0.50	0.50	0.50	0.50
Na <sub>2</sub> O	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Fe <sub>2</sub> O <sub>3</sub>	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25
B <sub>2</sub> O <sub>3</sub>	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
SiO <sub>2</sub> /RO	2.27	2.20	2.14	2.22	2.17	2.17	2.16	2.09	2.03	2.00
T <sub>FORM</sub> (°C)	1237	1230	1220	1227	1218	1228	1197	1222	1209	1206
T <sub>LIQ</sub> (°C)	1149	1141	1131	1131	1131	1141	1156	1137	1168	1169
ΔT (°C)	86	89	89	96	87	87	41	85	41	37

- 12 -

TABLE B - TYPE I-2 AND II-2 GLASS (cont'd)

Composition Weight %	Examples								
	75	76	77	78	79	80	81	82	83
SiO <sub>2</sub>	56.75	56.15	56.25	58.61	59.01	58.70	57.75	59.05	59.11
Al <sub>2</sub> O <sub>3</sub>	13.20	13.05	13.20	12.16	12.04	13.35	13.20	12.20	12.16
CaO	22.25	23.00	23.25	23.50	23.27	23.50	23.25	23.95	23.00
MgO	2.55	2.55	2.55	2.50	2.48	2.50	2.50	2.55	2.50
TiO <sub>2</sub>	1.10	1.10	1.10	1.10	1.09	0.50	1.10	1.10	1.10
Na <sub>2</sub> O	0.90	0.90	0.90	0.90	0.89	0.30	0.90	0.90	0.90
Fe <sub>2</sub> O <sub>3</sub>	0.25	0.25	0.25	0.23	0.23	0.25	0.25	0.25	0.23
B <sub>2</sub> O <sub>3</sub>	3.00	3.00	3.00	1.00	1.00	0.90	1.00	1.00	1.00
SiO <sub>2</sub> /RO	2.29	2.20	2.18	2.25	2.29	2.26	2.24	2.23	2.32
T <sub>FORM</sub> (°C)	1221	1212	1214	1242	1252	1253	1250	1254	1248
T <sub>LIQ</sub> (°C)	1121	1178	1114	1161	1178	1145	1154	1183	1152
ΔT (°C)	100	34	100	81	74	108	96	71	96

- 13 -

TABLE C – TYPE III-1 GLASS

Composition Weight %	Examples									
	84	85	86	87	88	89	90	91	92	93
SiO <sub>2</sub>	58.70	58.70	58.35	58.25	58.86	58.76	57.95	57.65	58.96	58.15
Al <sub>2</sub> O <sub>3</sub>	13.35	13.35	13.20	13.40	13.44	13.64	13.20	13.40	13.24	13.20
CaO	23.50	23.50	23.65	23.55	23.55	23.45	24.05	24.15	23.65	23.85
MgO	2.50	2.50	2.55	2.55	2.50	2.50	2.55	2.55	2.50	2.55
TiO <sub>2</sub>	0.50	0.50	1.10	1.10	0.50	0.50	1.10	1.10	0.50	1.10
Na <sub>2</sub> O	0.60	0.30								
Li <sub>2</sub> O	0.60	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Fe <sub>2</sub> O <sub>3</sub>	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25
SiO <sub>2</sub> /RO	2.26	2.26	2.23	2.23	2.26	2.26	2.18	2.16	2.25	2.20
T <sub>FORM</sub> (°C)	1226	1211	1211	1215	1216	1218	1205	1206	1212	1237
T <sub>LIQ</sub> (°C)	1157	1153	1146	1153	1153	1150	1151	1154	1158	1172
ΔT (°C)	69	58	65	62	63	68	54	52	54	65

TABLE C – TYPE III-1 GLASS (cont'd)

Composition Weight %	Examples									
	94	95	96	97	98	99	100	101	102	103
SiO <sub>2</sub>	59.61	59.97	60.09	60.21	60.33	59.61	59.61	59.73	59.85	59.97
Al <sub>2</sub> O <sub>3</sub>	12.12	12.19	12.22	12.24	12.27	12.92	12.92	12.92	12.95	12.97
CaO	22.12	23.56	23.31	23.35	23.40	21.91	21.96	22.00	22.04	22.09
MgO	3.50	2.90	2.70	2.50	2.30	3.50	3.30	3.10	2.90	2.70
TiO <sub>2</sub>	0.50	0.50	0.50	0.50	0.50	1.10	1.10	1.10	1.10	1.10
Na <sub>2</sub> O										
Li <sub>2</sub> O	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Fe <sub>2</sub> O <sub>3</sub>	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25
SiO <sub>2</sub> /RO	2.33	2.27	2.31	2.33	2.35	2.35	2.36	2.38	2.40	2.42
T <sub>FORM</sub> (°C)	1205	1207	1217	1213	1216	1213	1213	1214	1214	1219
T <sub>LIQ</sub> (°C)	1190	1170	1163	1162	1166	1179	1170	1164	1161	1160
ΔT (°C)	15	37	54	51	50	34	43	50	53	59

- 14 -

TABLE C – TYPE III-1 GLASS (cont'd)

Composition Weight %	Examples									
	104	105	106	107	108	109	110	111	112	113
SiO <sub>2</sub>	60.09	60.21	60.00	60.57	59.80	59.75	59.65	59.60	59.55	59.50
Al <sub>2</sub> O <sub>3</sub>	13.00	13.02	12.50	13.10	12.25	12.25	12.25	12.25	12.25	12.25
CaO	22.13	22.18	23.70	22.31	22.60	22.85	23.35	23.60	23.85	24.10
MgO	2.50	2.30	1.90	1.70	3.10	2.90	2.50	2.30	2.10	1.90
TiO <sub>2</sub>	1.10	1.10	1.10	1.10	1.10	1.10	1.10	1.10	1.10	1.10
Na <sub>2</sub> O					0.30	0.30	0.30	0.30	0.30	0.30
Li <sub>2</sub> O	0.90	0.90	0.90	0.90	0.60	0.60	0.60	0.60	0.60	0.60
Fe <sub>2</sub> O <sub>3</sub>	0.25	0.25	0.25	0.25						
SiO <sub>2</sub> /RO	2.44	2.46	2.34	2.52	2.33	2.32	2.31	2.30	2.29	2.29
T <sub>FORM</sub> (°C)	1223	1233	1239	1239	1240	1236	1236	1238	1234	1234
T <sub>LIQ</sub> (°C)	1155	1142	1139	1141	1156	1156	1159	1167	1173	1181
ΔT (°C)	68	91	100	98	94	80	77	71	61	53

TABLE C – TYPE III-1 GLASS (cont'd)

Composition Weight %	Examples									
	114	115	116	117	118	119	120	121	122	123
SiO <sub>2</sub>	59.45	60.00	59.95	59.90	59.85	59.61	59.97	60.09	60.21	60.33
Al <sub>2</sub> O <sub>3</sub>	12.25	12.40	12.40	12.40	12.0	12.12	12.19	12.22	12.24	12.27
CaO	24.35	22.05	23.30	23.55	23.80	22.12	22.25	22.30	22.34	22.39
MgO	1.70	2.30	2.10	1.90	1.70	3.50	2.90	2.70	2.50	2.30
TiO <sub>2</sub>	1.10	1.10	1.10	1.10	1.10	1.50	1.50	1.50	1.50	1.50
Na <sub>2</sub> O	0.30									
Li <sub>2</sub> O	0.60	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Fe <sub>2</sub> O <sub>3</sub>		0.25	0.25	0.26	0.25	0.25	0.25	0.25	0.25	0.25
SiO <sub>2</sub> /RO	2.28	2.46	2.36	2.35	2.35	2.33	2.38	2.40	2.42	2.44
T <sub>FORM</sub> (°C)	1234	1230	1231	1224	1224	1215	1217	1213	1215	1231
T <sub>LIQ</sub> (°C)	1192	1146	1152	1156	1156	1181	1161	1178	1162	1160
ΔT (°C)	42	84	79	68	68	34	56	35	53	71



- 15 -

TABLE C – TYPE III-1 GLASS (cont'd)

Composition Weight %	Examples									
	124	125	126	127	128	129	130	131	132	133
SiO <sub>2</sub>	60.75	60.21	59.78	58.70	57.75	58.05	57.85	59.71	59.46	60.02
Al <sub>2</sub> O <sub>3</sub>	12.35	13.02	12.30	13.35	13.20	13.40	13.40	13.24	13.24	12.35
CaO	22.55	22.52	23.26	23.50	24.25	23.75	23.95	22.90	23.15	23.35
MgO	1.70	2.50	2.53	2.50	2.55	2.55	2.55	2.50	2.50	2.54
TiO <sub>2</sub>	1.50	0.50	0.50	0.50	1.10	1.10	1.10	0.50	0.50	0.50
Na <sub>2</sub> O		0.00								
Li <sub>2</sub> O	0.90	1.00	1.40	1.20	0.90	0.90	0.90	0.90	0.90	1.00
Fe <sub>2</sub> O <sub>3</sub>	0.25	0.25	0.23	0.25	0.25	0.25	0.25	0.25	0.25	0.23
SiO <sub>2</sub> /RO	2.51	2.41	2.32	2.26	2.15	2.21	2.18	2.35	2.32	2.32
T <sub>FORM</sub> (°C)	1240	1231	1187	1194	1201	1202	1199	1227	1226	1209
T <sub>LIQ</sub> (°C)	1166	1143	1158	1149	1155	1153	1157	1142	1147	1159
ΔT (°C)	74	88	29	45	46	49	42	85	79	50

TABLE C – TYPE III-1 GLASS (cont'd)

Composition Weight %	Examples									
	134	135	136	137	138	139	140	141	142	143
SiO <sub>2</sub>	59.90	60.26	60.14	59.16	60.10	60.23	60.10	60.23	59.78	60.14
Al <sub>2</sub> O <sub>3</sub>	12.32	12.40	12.37	13.24	13.00	12.25	13.00	12.25	12.30	12.37
CaO	23.31	23.45	23.40	23.45	22.15	23.36	22.15	23.36	23.26	23.40
MgO	2.53	2.55	2.54	2.50	2.50	2.50	2.50	2.50	2.53	2.54
TiO <sub>2</sub>	0.50	0.51	0.51	0.50	1.10	0.51	1.10	0.51	0.50	0.51
Na <sub>2</sub> O										
Li <sub>2</sub> O	1.20	0.60	0.80	0.90	0.90	0.90	0.90	0.90	1.40	0.80
Fe <sub>2</sub> O <sub>3</sub>	0.23	0.23	0.23	0.25	0.25	0.25	0.25	0.25	0.23	0.23
SiO <sub>2</sub> /RO	2.32	2.32	2.32	2.28	2.44	2.33	2.44	2.33	2.32	2.32
T <sub>FORM</sub> (°C)	1199	1230	1219	1218	1235	1220	1237	1224	1198	1219
T <sub>LIQ</sub> (°C)	1160	1158	1159	1156	1133	1160	1136	1158	1156	1159
ΔT (°C)	39	72	60	62	102	60	101	66	42	60

- 16 -

TABLE C – TYPE III-1 GLASS (cont'd)

Composition Weight %	Examples							
	144	145	146	147	148	149	150	151
SiO <sub>2</sub>	60.38	60.33	59.70	60.21	60.21	60.21	60.50	58.70
Al <sub>2</sub> O <sub>3</sub>	12.42	13.05	12.25	13.02	13.02	13.02	12.45	13.35
CaO	23.50	22.22	22.85	22.52	22.52	22.52	23.54	23.50
MgO	2.55	2.10	2.70	2.50	2.50	2.50	2.56	2.50
TiO <sub>2</sub>	0.51	1.10	1.10	0.50	0.50	0.50	0.51	0.50
Na <sub>2</sub> O			0.30	0.25	0.50	0.75		0.90
Li <sub>2</sub> O	0.40	0.90	0.60	0.75	0.50	0.25	0.20	0.30
Fe <sub>2</sub> O <sub>3</sub>	0.23	0.25		0.25	0.25	0.25	0.24	0.25
SiO <sub>2</sub> /RO	2.32	2.48	2.34	2.41	2.41	2.41	2.32	2.26
T <sub>FORM</sub> (°C)	1244	1258	1242	1242	1253	1263	1256	1241
T <sub>LIQ</sub> (°C)	1158	1136	1155	1147	1152	1160	1158	1165
ΔT (°C)	86	122	87	95	101	103	98	76

TABLE C – TYPE III-1 GLASS (cont'd)

Composition Weight %	Examples				
	152	153	154	155	156*
SiO <sub>2</sub>	60.05	60.05	60.05	59.30	59.30
Al <sub>2</sub> O <sub>3</sub>	12.98	12.98	12.98	12.10	12.10
CaO	22.14	22.14	22.14	22.60	22.60
MgO	3.12	3.12	3.12	3.40	3.40
TiO <sub>2</sub>	0.55	0.55	0.55	1.50	1.50
Na <sub>2</sub> O				0.45	
Li <sub>2</sub> O	0.91	0.91	0.91	0.45	0.90
Fe <sub>2</sub> O <sub>3</sub>	0.25	0.25	0.25	0.20	0.20
SiO <sub>2</sub> /RO	2.38	2.38	2.38	2.28	2.28
T <sub>FORM</sub> (°C) (NIST 710A)	1214	1219	1223	1218	1191
T <sub>LIQ</sub> (°C)	1159	1164	1163	1179	1187
ΔT (°C)	55	55	60	39	4

\* composition included 0.50 wt% BaO

TABLE D – TYPE III-2 GLASS

Composition Weight %	Examples									
	157	158	159	160	161	162	163	164	165	166
SiO <sub>2</sub>	58.25	58.30	58.20	58.10	58.00	58.15	58.15	58.10	57.35	57.95
Al <sub>2</sub> O <sub>3</sub>	13.33	13.03	13.03	13.03	13.03	13.20	13.33	13.63	13.20	13.20
CaO	23.29	23.54	23.64	23.74	23.84	22.85	23.39	23.14	23.65	24.05
MgO	2.50	2.50	2.50	2.50	2.50	2.55	2.50	2.50	2.55	2.55
TiO <sub>2</sub>	0.50	0.50	0.50	0.50	0.50	1.10	0.50	0.50	1.10	1.10
Na <sub>2</sub> O										
Li <sub>2</sub> O	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
ZnO	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Fe <sub>2</sub> O <sub>3</sub>	0.23	0.23	0.23	0.23	0.23	0.25	0.23	0.23	0.25	0.25
SiO <sub>2</sub> /RO	2.26	2.24	2.23	2.21	2.20	2.29	2.25	2.26	2.19	2.18
T <sub>FORM</sub> (°C)	1213	1204	1205	1206	1208	1207	1208	1212	1195	1195
T <sub>LIQ</sub> (°C)	1146	1147	1148	1144	1149	1136	1152	1157	1141	1140
ΔT (°C)	67	57	57	62	59	71	56	55	54	55

TABLE D – TYPE III-2 GLASS (cont'd)

Composition Weight %	Examples									
	167	168	169	170	171	172	173	174	175	176
SiO <sub>2</sub>	59.61	59.47	59.12	57.75	58.00	59.73	59.85	59.97	60.09	60.21
Al <sub>2</sub> O <sub>3</sub>	12.16	12.16	12.00	13.20	13.63	12.92	12.95	12.97	13.00	13.02
CaO	23.50	24.22	22.50	24.25	23.24	22.00	22.04	22.09	22.13	22.18
MgO	2.50	1.90	3.40	2.55	2.50	3.10	2.90	2.70	2.50	2.30
TiO <sub>2</sub>	1.10	1.10	1.00	1.10	0.50	1.10	1.10	1.10	1.10	1.10
Na <sub>2</sub> O										
Li <sub>2</sub> O	0.45	0.45	0.90	0.90	0.90	0.45	0.45	0.45	0.45	0.45
ZnO	0.45	0.45	1.00	1.00	1.00	0.45	0.45	0.45	0.45	0.45
Fe <sub>2</sub> O <sub>3</sub>			0.20	0.25	0.23	0.25	0.25	0.25	0.25	0.25
SiO <sub>2</sub> /RO	2.29	2.28	2.28	2.15	2.25	2.38	2.40	2.42	2.44	2.46
T <sub>FORM</sub> (°C)	1229	1218	1190	1194	1212	1242	1246	1246	1251	1251
T <sub>LIQ</sub> (°C)	1154	1159	1163	1159	1163	1173	1168	1154	1147	1144
ΔT (°C)	75	59	27	35	49	69	78	92	104	107

TABLE D – TYPE III-2 GLASS (cont'd)

Composition Weight %	Examples						
	177	178	179	180	181	182	183
SiO <sub>2</sub>	60.33	60.45	60.57	59.40	59.20	59.54	59.40
Al <sub>2</sub> O <sub>3</sub>	13.05	13.08	13.10	12.16	12.16	12.16	12.16
CaO	22.22	22.27	22.31	23.49	23.69	23.95	24.49
MgO	2.10	1.90	1.70	2.30	2.30	2.10	1.70
TiO <sub>2</sub>	1.10	1.10	1.10	1.10	1.10	1.10	1.10
Na <sub>2</sub> O				0.40	0.40		
Li <sub>2</sub> O	0.45	0.45	0.45	0.45	0.45	0.45	0.45
ZnO	0.45	0.45	0.45	0.45	0.45	0.45	0.45
Fe <sub>2</sub> O <sub>3</sub>	0.25	0.25	0.25				
SiO <sub>2</sub> /RO	2.48	2.50	2.52	2.30	2.28	2.29	2.27
T <sub>FORM</sub> (°C)	1260	1260	1263	1245	1247	1241	1245
T <sub>LIQ</sub> (°C)	1140	1139	1135	1159	1152	1155	1168
ΔT (°C)	120	121	128	86	95	86	77

- 19 -

TABLE E – TYPE III-3 GLASS

Composition Weight %	Examples									
	184	185	186	187	188	189	190	191	192	193
SiO <sub>2</sub>	59.73	59.85	59.97	60.09	60.21	60.33	60.45	60.57	58.80	58.70
Al <sub>2</sub> O <sub>3</sub>	12.92	12.95	12.97	13.00	13.02	13.05	13.08	13.10	13.00	11.90
CaO	22.00	22.04	22.09	22.13	22.18	22.22	22.27	22.31	23.45	22.40
MgO	3.10	2.90	2.70	2.50	2.30	2.10	1.90	1.70	2.50	3.40
TiO <sub>2</sub>	1.10	1.10	1.10	1.10	1.10	1.10	1.10	1.10	1.10	1.50
ZnO	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	1.00
Na <sub>2</sub> O										0.90
K <sub>2</sub> O										
Fe <sub>2</sub> O <sub>3</sub>	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.20
SiO <sub>2</sub> /RO	2.38	2.40	2.42	2.44	2.46	2.48	2.50	2.52	2.27	2.28
T <sub>FORM</sub> (°C)	1265	1267	1273	1278	1273	1280	1285	1275	1268	1226
T <sub>LIQ</sub> (°C)	1170	1166	1159	1157	1166	1169	1170	1171	1165	1180
ΔT (°C)	95	101	114	121	107	111	115	104	103	46

TABLE E – TYPE III-3 GLASS (cont'd)

Composition Weight %	Examples			
	194	195	196	197
SiO <sub>2</sub>	59.00	58.70	58.19	59.00
Al <sub>2</sub> O <sub>3</sub>	12.00	11.90	11.84	12.00
CaO	22.50	22.40	21.33	22.50
MgO	3.40	3.40	2.82	3.40
TiO <sub>2</sub>	1.00	1.00	1.86	1.50
ZnO	1.00	1.50	2.28	0.50
Na <sub>2</sub> O	0.90	0.90	1.18	0.90
K <sub>2</sub> O			0.16	
Fe <sub>2</sub> O <sub>3</sub>	0.20	0.20	0.24	0.20
SiO <sub>2</sub> /RO	2.28	2.28	2.24	2.28
T <sub>FORM</sub> (°C) (NIST 710A)	1234	1231	1212	1230
T <sub>LIQ</sub> (°C)	1175	1181	1159	1183
ΔT (°C)	69	50	53	37

- 20 -

TABLE F – TYPE III-4 GLASS

Composition Weight %	Examples									
	198	199	200	201	202	203	204	205	206	207
SiO <sub>2</sub>	58.00	57.90	57.80	58.15	58.25	58.00	58.10	58.30	58.20	58.10
Al <sub>2</sub> O <sub>3</sub>	13.43	13.43	13.43	13.33	13.33	13.63	13.63	13.03	13.03	13.03
CaO	23.44	23.54	23.64	23.39	23.29	23.24	23.14	23.54	23.64	23.74
MgO	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50
TiO <sub>2</sub>	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
B <sub>2</sub> O <sub>3</sub>	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Na <sub>2</sub> O										
K <sub>2</sub> O										
Li <sub>2</sub> O	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Fe <sub>2</sub> O <sub>3</sub>	0.23	0.23	0.23	0.23	0.23	0.23	0.23	0.23	0.23	0.23
SiO <sub>2</sub> /RO	2.24	2.22	2.21	2.25	2.26	2.25	2.27	2.24	2.23	2.21
T <sub>FORM</sub> (°C)	1202	1203	1197	1203	1202	1207	1212	1200	1201	1194
T <sub>LIQ</sub> (°C)	1139	1137	1139	1136	1145	1144	1146	1132	1137	1135
ΔT (°C)	63	66	58	67	57	63	66	68	64	59

TABLE F – TYPE III-4 GLASS (cont'd)

Composition Weight %	Examples									
	208*	209*	210*	211	212	213	214	215	216	217
SiO <sub>2</sub>	58.74	58.64	58.64	58.75	58.00	57.80	57.60	57.60	57.60	57.60
Al <sub>2</sub> O <sub>3</sub>	13.05	13.15	12.95	12.93	13.03	13.23	13.23	13.23	13.23	13.03
CaO	22.97	22.97	22.87	22.93	23.84	23.84	23.84	23.84	23.84	24.04
MgO	2.36	2.36	2.36	2.36	2.50	2.50	2.50	2.50	2.50	2.50
TiO <sub>2</sub>	0.49	0.49	0.49	0.50	0.50	0.50	0.50	0.50	0.50	0.50
B <sub>2</sub> O <sub>3</sub>	1.00	1.00	1.00	1.20	1.00	1.00	1.20	1.20	1.20	1.20
Na <sub>2</sub> O				0.04				0.10	0.20	0.20
K <sub>2</sub> O	0.09	0.09	0.09	0.10						
Li <sub>2</sub> O	0.91	0.91	0.91	0.90	0.90	0.90	0.90	0.80	0.70	0.70
Fe <sub>2</sub> O <sub>3</sub>	0.29	0.29	0.29	0.29	0.23	0.23	0.23	0.23	0.23	0.23
SiO <sub>2</sub> /RO	2.32	2.32	2.32	2.32	2.20	2.19	2.19	2.19	2.19	2.17
T <sub>FORM</sub> (°C)	1210	1209	1204	1210	1198	1201	1200	1196	1208	1201
T <sub>LIQ</sub> (°C)	1145	1151	1142	1127	1138	1126	1125	1133	1135	1145
ΔT (°C)	65	58	62	83	60	75	75	63	73	56

\* compositions include 0.05 wt% SrO and 0.08 wt% SO<sub>3</sub>

- 21 -

TABLE F – TYPE III-4 GLASS (cont'd)

Composition Weight %	Examples									
	218	219	220	221	222	223	224	225	226	227
SiO <sub>2</sub>	58.50	58.40	58.30	58.40	58.15	58.25	58.70	58.00	57.60	58.00
Al <sub>2</sub> O <sub>3</sub>	12.76	12.76	13.03	13.03	13.33	13.33	12.75	13.03	13.03	13.03
CaO	23.61	23.71	23.54	23.44	23.39	23.29	23.50	23.84	24.04	23.84
MgO	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50
TiO <sub>2</sub>	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
B <sub>2</sub> O <sub>3</sub>	1.00	1.00	1.00	1.00	1.00	1.00	0.60	1.00	1.20	1.00
Na <sub>2</sub> O							0.60			
K <sub>2</sub> O										
Li <sub>2</sub> O	0.90	0.90	0.90	0.90	0.90	0.90	0.60	0.90	0.90	0.90
Fe <sub>2</sub> O <sub>3</sub>	0.23	0.23	0.23	0.23	0.25	0.25	0.25	0.23	0.23	0.23
SiO <sub>2</sub> /RO	2.24	2.23	2.24	2.25	2.25	2.26	2.26	2.20	2.17	2.20
T <sub>FORM</sub> (°C)	1202	1203	1201	1208	1197	1200	1216	1202	1194	1192
T <sub>LIQ</sub> (°C)	1141	1145	1138	1137	1130	1134	1160	1137	1142	1137
ΔT (°C)	61	58	63	71	67	66	56	65	52	55

TABLE F – TYPE III-4 GLASS (cont'd)

Composition Weight %	Examples									
	228	229	230	231	232	233	234	235	236	237
SiO <sub>2</sub>	58.61	58.61	58.00	57.90	58.11	58.40	58.40	58.50	58.60	58.00
Al <sub>2</sub> O <sub>3</sub>	12.16	12.16	13.23	13.23	13.36	13.36	13.03	13.03	13.03	13.63
CaO	23.50	23.50	23.64	23.74	23.40	23.11	23.44	23.34	23.24	23.24
MgO	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50
TiO <sub>2</sub>	1.10	1.10	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
B <sub>2</sub> O <sub>3</sub>	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Na <sub>2</sub> O		0.45								
K <sub>2</sub> O										
Li <sub>2</sub> O	0.90	0.45	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Fe <sub>2</sub> O <sub>3</sub>	0.23	0.23	0.23	0.23	0.23	0.23	0.23	0.23	0.23	0.23
SiO <sub>2</sub> /RO	2.25	2.25	2.22	2.21	2.24	2.28	2.25	2.26	2.28	2.25
T <sub>FORM</sub> (°C)	1201	1227	1201	1195	1196	1204	1201	1204	1204	1206
T <sub>LIQ</sub> (°C)	1142	1159	1135	1137	1133	1133	1136	1133	1135	1136
ΔT (°C)	59	68	66	58	63	71	65	71	69	70

- 22 -

TABLE F – TYPE III-4 GLASS (cont'd)

Composition Weight %	Examples									
	238	239	240	241	242	243	244	245	246	247
SiO <sub>2</sub>	58.10	58.10	58.70	58.70	58.70	58.61	58.40	58.80	58.30	57.60
Al <sub>2</sub> O <sub>3</sub>	13.23	13.43	12.75	12.35	12.35	12.16	12.76	12.46	13.03	13.03
CaO	23.54	23.34	23.50	23.50	23.50	23.50	23.71	23.61	23.54	24.04
MgO	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50
TiO <sub>2</sub>	0.50	0.50	0.50	0.50	0.50	1.10	0.50	0.50	0.50	0.50
B <sub>2</sub> O <sub>3</sub>	1.00	1.00	0.60	1.00	1.00	1.00	1.00	1.00	1.00	1.20
Na <sub>2</sub> O			0.30	0.60	0.30					0.10
K <sub>2</sub> O										
Li <sub>2</sub> O	0.90	0.90	0.90	0.60	0.90	0.90	0.90	0.90	0.90	0.80
Fe <sub>2</sub> O <sub>3</sub>	0.23	0.23	0.25	0.25	0.25	0.23	0.23	0.23	0.23	0.23
SiO <sub>2</sub> /RO	2.23	2.25	2.26	2.26	2.26	2.25	2.23	2.25	2.24	2.17
T <sub>FORM</sub> (°C)	1199	1204	1204	1207	1202	1194	1194	1195	1195	1196
T <sub>LIQ</sub> (°C)	1133	1134	1153	1157	1149	1141	1144	1145	1140	1145
ΔT (°C)	63	70	51	50	53	53	50	50	55	51

TABLE F – TYPE III-4 GLASS (cont'd)

Composition Weight %	Examples									
	248	249	250	251	252	253	254	255	256	257
SiO <sub>2</sub>	58.50	58.11	58.91	58.11	58.30	58.20	58.10	58.70	58.70	58.11
Al <sub>2</sub> O <sub>3</sub>	12.76	13.36	12.16	13.36	13.03	13.03	13.03	13.35	13.35	13.36
CaO	23.61	23.40	23.80	23.40	23.54	23.64	23.74	23.50	23.50	23.40
MgO	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50
TiO <sub>2</sub>	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
B <sub>2</sub> O <sub>3</sub>	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.30	0.60	1.00
Na <sub>2</sub> O										
K <sub>2</sub> O										
Li <sub>2</sub> O	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.60	0.90
Fe <sub>2</sub> O <sub>3</sub>	0.23	0.23	0.23	0.23	0.23	0.23	0.23	0.25	0.25	0.23
SiO <sub>2</sub> /RO	2.24	2.24	2.24	2.24	2.24	2.23	2.21	2.26	2.26	2.24
T <sub>FORM</sub> (°C)	1197	1229	1216	1213	1202	1202	1205	1207	1224	1212
T <sub>LIQ</sub> (°C)	1139	1155	1148	1142	1136	1136	1137	1144	1145	1135
ΔT (°C)	58	133	123	126	120	119	122	114	142	139



- 23 -

TABLE F – TYPE III-4 GLASS (cont'd)

Composition Weight %	Examples									
	258	259	260	261	262	263	264	265	266	267
SiO <sub>2</sub>	58.20	58.70	59.53	59.61	59.11	59.11	59.16	59.21	57.80	59.11
Al <sub>2</sub> O <sub>3</sub>	13.23	12.35	12.25	12.16	12.16	12.16	12.16	12.16	13.03	12.16
CaO	23.44	23.50	23.17	23.50	23.00	23.00	23.20	23.40	24.04	23.50
MgO	2.50	2.50	2.52	2.50	2.50	2.50	2.25	2.00	2.50	2.00
TiO <sub>2</sub>	0.50	0.50	0.50	1.10	1.10	1.10	1.10	1.10	0.50	1.10
B <sub>2</sub> O <sub>3</sub>	1.00	1.00	1.00	0.45	1.00	1.00	1.00	1.00	1.00	1.00
Na <sub>2</sub> O										
K <sub>2</sub> O										
Li <sub>2</sub> O	0.90	1.20	0.80	0.45	0.90	0.90	0.90	0.90	0.90	0.90
Fe <sub>2</sub> O <sub>3</sub>	0.23	0.25	0.23	0.23	0.23	0.23	0.23	0.23	0.23	0.23
SiO <sub>2</sub> /RO	2.24	2.26	2.32	2.29	2.32	2.32	2.32	2.33	2.18	2.32
T <sub>FORM</sub> (°C)	1204	1187	1214	1230	1205	1216	1218	1213	1196	1209
T <sub>LIQ</sub> (°C)	1135	1147	1143	1155	1142	1143	1147	1153	1147	1153
ΔT (°C)	124	40	71	75	63	73	71	60	49	56

TABLE F – TYPE III-4 GLASS (cont'd)

Composition Weight %	Examples									
	268	269	270	271	272	273	274	275	276	277
SiO <sub>2</sub>	59.36	59.31	59.36	59.41	59.11	59.16	59.21	59.16	59.11	59.01
Al <sub>2</sub> O <sub>3</sub>	12.41	12.56	12.51	12.46	12.16	12.16	12.16	12.26	12.26	12.36
CaO	23.60	23.50	23.50	23.50	23.00	23.20	23.40	23.45	23.50	23.50
MgO	2.00	2.00	2.00	2.00	2.50	2.25	2.00	2.50	2.50	2.50
TiO <sub>2</sub>	0.50	0.50	0.50	0.50	1.10	1.10	1.10	0.50	0.50	0.50
B <sub>2</sub> O <sub>3</sub>	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Na <sub>2</sub> O										
K <sub>2</sub> O										
Li <sub>2</sub> O	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Fe <sub>2</sub> O <sub>3</sub>	0.23	0.23	0.23	0.23	0.23	0.23	0.23	0.23	0.23	0.23
SiO <sub>2</sub> /RO	2.32	2.33	2.33	2.33	2.32	2.32	2.33	2.28	2.27	2.27
T <sub>FORM</sub> (°C)	1216	1220	1220	1220	1216	1214	1220	1209	1210	1210
T <sub>LIQ</sub> (°C)	1153	1153	1158	1155	1144	1147	1158	1150	1152	1152
ΔT (°C)	63	67	62	65	72	67	62	59	58	58

- 24 -

TABLE F – TYPE III-4 GLASS (cont'd)

Composition Weight %	Examples									
	278	279	280	281	282	283	284	285	286	287
SiO <sub>2</sub>	58.91	58.91	59.21	58.31	58.61	58.70	58.60	58.50	58.75	58.75
Al <sub>2</sub> O <sub>3</sub>	12.36	12.16	12.16	12.16	12.76	12.46	12.46	12.46	12.93	12.93
CaO	23.60	23.80	23.50	24.40	23.50	23.71	23.81	23.91	22.93	22.93
MgO	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.50	2.36	2.36
TiO <sub>2</sub>	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
B <sub>2</sub> O <sub>3</sub>	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.20	1.20
Na <sub>2</sub> O									0.14	0.24
K <sub>2</sub> O									0.10	0.10
Li <sub>2</sub> O	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.80	0.70
Fe <sub>2</sub> O <sub>3</sub>	0.23	0.23	0.23	0.23	0.23	0.23	0.23	0.23	0.29	0.29
SiO <sub>2</sub> /RO	2.26	2.28	2.28	2.17	2.25	2.24	2.23	2.22	2.32	2.32
T <sub>FORM</sub> (°C)	1196	1196	1201	1195	1183	1193	1192	1191	1211	1218
T <sub>LIQ</sub> (°C)	1152	1156	1143	1151	1165	1152	1151	1152	1127	1129
ΔT (°C)	44	40	58	44	18	41	41	39	84	89

TABLE F – TYPE III-4 GLASS (cont'd)

Composition Weight %	Examples										
	288	289	290	291	292	293	294	295	296	297	298
SiO <sub>2</sub>	58.50	58.70	58.70	58.10	58.70	58.91	59.11	59.31	59.21	60.12	59.11
Al <sub>2</sub> O <sub>3</sub>	12.34	13.05	12.75	13.63	13.35	12.16	12.16	12.26	12.26	13.00	12.16
CaO	23.70	23.50	23.50	23.14	23.50	23.80	23.50	22.30	23.40	21.13	23.00
MgO	2.50	2.50	2.50	2.50	2.50	2.50	2.00	2.50	2.50	2.50	2.50
TiO <sub>2</sub>	0.50	0.50	0.50	0.50	0.50	0.50	1.10	0.50	0.50	1.10	1.10
B <sub>2</sub> O <sub>3</sub>	1.20	0.30	0.60	1.00	0.90	1.00	1.00	1.00	1.00	1.00	1.00
Na <sub>2</sub> O											0.45
K <sub>2</sub> O	0.08										
Li <sub>2</sub> O	0.90	.20	1.20	0.90	0.30	0.90	0.90	0.90	0.90	0.90	0.45
Fe <sub>2</sub> O <sub>3</sub>	0.28	0.25	0.25	0.23	0.25	0.23	0.23	0.23	0.23	0.25	0.23
SiO <sub>2</sub> /RO	2.23	2.26	2.26	2.27	2.26	2.24	2.32	2.39	2.29	2.54	2.32
T <sub>FORM</sub> (°C)	1195	1196	1195	1204	1239	1197	1215	1209	1210	1285	1243
T <sub>LIQ</sub> (°C)	1151	1147	1147	1115	1143	1155	1155	1148	1156	1189	1149
ΔT (°C)	44	49	48	89	96	42	60	61	54	96	94

- 25 -

The samples were experimental samples produced in a laboratory. The experimental samples were prepared from reagent grade oxides (e.g., pure silica or calcia). The batch size for each example was 1000 grams. The individual batch ingredients were weighed out, combined and placed in a tightly sealed glass jar or plastic container. The sealed jar or container was then placed in a paint shaker for 15 minutes or in a turbular mixer for 25 minutes to effectively mix the ingredients. A portion of the batch was then placed into a platinum crucible, filling no more than 3/4 of its volume. The crucible was then placed in a furnace and heated to 1427°C (2600°F) for 15 minutes. The remaining batch was then added to the hot crucible and heated to 1427°C (2600°F) for 15 to 30 minutes. The furnace temperature was then raised to 1482°C (2700°F) and held there for 2 hours. The molten glass was then fritted in water and dried. The fritted samples were remelted at 1482°C (2700°F) and held there for 2 hours. The molten glass was then fritted again in water and dried. The forming temperature, i.e. the glass temperature at a viscosity of 1000 poise, was determined by ASTM method C965-81, and the liquidus temperature by ASTM method C829-81.

The weight percent of the constituents of the compositions shown in Tables A through F are based on the weight percent of each constituent in the batch. It is believed that the batch weight percent is generally about the same as the weight percent of the melted sample, except for glass batch materials that volatilize during melting, e.g. boron and fluorine. For boron, it is believed that the weight percent of  $B_2O_3$  in a laboratory sample will be 5 to 15 percent less than the weight percent of  $B_2O_3$  in the batch composition, the precise loss depending on the composition and melting conditions. For fluorine, it is believed that the weight percent of fluorine in a laboratory test sample will be about 50 percent less than the weight percent of fluorine in the batch composition, the precise loss depending on the composition and melting conditions. It is further believed that glass fiber compositions made from commercial grade materials and melted under conventional operating conditions will have similar batch and melt weight percents as discussed above, with the precise loss depending, in part, on the furnace operating temperature, through-put and quality of commercial batch materials. The amount of boron and fluorine reported in the tables takes into consideration the expected loss of these materials and represents the expected amount of the material in the glass composition.

- 26 -

Determination of the log 3 forming temperature was based on the glass samples being compared against physical standards supplied by the National Institute of Standards and Testing (NIST). In Tables A through F, the reported log 3 forming temperature is based on comparison to either NIST 710A or NIST 714, both of which are a soda lime silica glass standard. It is expected that both standards will provide comparable results since both are based on a soda lime silica standard. The  $T_{UQ}$  is unaffected by the NIST standard. Unless otherwise stated, the log 3 forming temperatures reported herein are based on the NIST 714 standard.

In the present invention, the compositional variables of interest are the weight percent  $\text{SiO}_2$  and weight percent RO, and the relationship of interest is the ratio of  $\text{SiO}_2$  to RO, i.e.  $\text{SiO}_2/\text{RO}$ . The melt properties of interest are the forming temperature and the liquidus temperature since one goal in the present invention is to provide a low boron glass composition having a lowered forming temperature and a desired  $\Delta T$  so that the composition can be processed at a lowered temperature while reducing the possibility of devitrification of the molten glass in the bushing area during a glass fiber forming operation. Without limiting the present invention, in one nonlimiting embodiment, the glass composition has a  $\Delta T$  of at least  $50^\circ\text{C}$  ( $90^\circ\text{F}$ ), e.g. at least  $55^\circ\text{C}$  ( $100^\circ\text{F}$ ). In other nonlimiting embodiments, the glass composition has a  $\Delta T$  of 50 to  $100^\circ\text{C}$  (90 to  $180^\circ\text{F}$ ), or 50 to  $83^\circ\text{C}$  (90 to  $150^\circ\text{F}$ ), or 50 to  $72^\circ\text{C}$  (90 to  $130^\circ\text{F}$ ).

Referring to Figures 1 through 6, the relationship between the  $\text{SiO}_2/\text{RO}$  ratio is plotted against both the forming temperature and liquidus temperature of the sample. The most suitable trendlines for the temperatures are based on a second-order-regression analysis protocol, and in particular are 2nd-order polynomial curves generated using Microsoft® Excel 97 SR-2(f). By inference, both trendlines also show the resulting change of the  $\Delta T$  between liquidus and forming temperatures.

In viewing Figures 1 through 6, it can be seen that as the  $\text{SiO}_2/\text{RO}$  ratio decreases, the forming temperature generally decreases, while the trend in the liquidus temperature differs depending on the glass type. In addition, it can be seen that as the  $\text{SiO}_2/\text{RO}$  ratio decreases,  $\Delta T$  also decreases. As a result, the  $\text{SiO}_2/\text{RO}$  ratio can be used to reduce the forming temperature of a glass fiber forming composition while providing a desired  $\Delta T$ . More particularly, in the present invention where  $\Delta T$  is at least  $50^\circ\text{C}$ , a composition having a  $\Delta T$  of  $50^\circ\text{C}$  is indicative of a

- 27 -

composition having a combination of materials and amounts that provides a minimum permissible forming temperature, i.e. the lowest forming temperature for the particular combination of constituents that still maintains the desired range between the forming and liquidus temperatures. From this, it can be inferred that the narrower the  $\Delta T$  range, the closer the glass forming temperature is to having the minimum permissible forming temperature for that particular combination of constituents. It can also be inferred that the further the  $\Delta T$  of a glass composition is from the minimum permissible  $\Delta T$ , the greater the opportunity to modify the glass composition in a manner that reduces  $T_{\text{FORM}}$  while maintaining a  $\Delta T$  no less than the minimum permissible  $\Delta T$ . To this end, the  $\text{SiO}_2/\text{RO}$  ratio can be manipulated by changing the amount of  $\text{SiO}_2$  and/or RO to produce a glass composition having a  $\Delta T$  as close as possible to the minimum desired  $\Delta T$ . It should be appreciated that if the  $\text{SiO}_2/\text{RO}$  ratio drops too low,  $\Delta T$  can drop to an unacceptable level. Although not required, in one nonlimiting embodiment of the present invention,  $\text{SiO}_2/\text{RO}$  is no greater than 2.35. In other nonlimiting embodiments,  $\text{SiO}_2/\text{RO}$  is no greater than 2.30, or no greater than 2.25, or no greater than 2.20. In still another nonlimiting embodiment of the invention,  $\text{SiO}_2/\text{RO}$  ranges from 1.9 to 2.3, e.g. 2.05 to 2.29.

Although Tables A through F and corresponding Figures 1 through 6 illustrate how the ratio of the weight percent of  $\text{SiO}_2$  to RO effects the melt properties of the glass, and in particular the liquidus temperature, forming temperature and  $\Delta T$ , additional glass sample compositions as well as additional relationships between the glass constituents, such as for example the difference in the amount of  $\text{SiO}_2$  and RO (i.e.  $\text{SiO}_2$  wt% - RO wt%), the weight percent of  $\text{Al}_2\text{O}_3$ , the ratio of  $\text{SiO}_2$  to  $\text{Al}_2\text{O}_3$ , and the ratio of RO to  $\text{Al}_2\text{O}_3$ , as they relate to liquidus and forming temperatures and  $\Delta T$ , are disclosed in U.S. Provisional Application No. 60/230474, which is incorporated herein by reference.

It is known that pure silica is the highest melting glass former. A pure silica melt does not have a well defined melting point, but gradually solidifies and forms a glass as it cools to room temperature and its viscosity drops from greater than  $\log 4$  (10,000) poise at  $2500^\circ\text{C}$  ( $1371^\circ\text{F}$ ). Pure calcia, magnesia and alumina melts are known to have very low viscosities of 0.5-2 poise at their respective melting points. These materials do not solidify into a glass but rather crystallize instantly at their sharply defined melting point. In a typical quaternary  $\text{SiO}_2\text{-Al}_2\text{O}_3\text{-CaO-MgO}$  glass

- 28 -

composition with 60% SiO<sub>2</sub> and 21% CaO, each oxide contributes its unique characteristics toward its balance of melt properties.

Based on these material properties, it can be inferred that as SiO<sub>2</sub>, which is the largest oxide component of the glass composition in terms of weight percent, is reduced in a given composition of this type, the melt viscosity and the resulting log 3 forming temperature drops. If CaO, which is the second largest component of the glass composition in terms of weight percent, is increased in such a composition, the effect of RO (CaO+MgO) on the glass properties will be twofold. More specifically, it will not only increase the fluidity of the resulting melt (i.e. decrease its viscosity) but it will also increase the crystallizability of the resulting melt (i.e. increase its liquidus temperature), and therefore reduce the  $\Delta T$ .

As a result, although not required, in one nonlimiting embodiment of the present invention, the glass compositions have (1) the lowest SiO<sub>2</sub> content that will yield the lowest log 3 forming temperatures, in combination with (2) the ratio of SiO<sub>2</sub> to RO (RO=CaO+MgO) that yields the process-required  $\Delta T$ , which in the present invention is at least 50°C.

Based on the above and although not required, in one nonlimiting embodiment of the present invention, the silica level is kept low, i.e. no greater than 59 wt% SiO<sub>2</sub>, in order to promote a lower log 3 forming temperature. In other nonlimiting embodiments of the present invention, the glass compositions have no greater than 58 wt% SiO<sub>2</sub>, or no greater than 57 wt% SiO<sub>2</sub>.

Table G summarizes features of selected low boron glass compositions disclosed in Tables A through F that have (i) a  $T_{\text{FORM}}$  of no greater than 1240°C (2264°F), (ii) a  $\Delta T$  in the range of 50-83°C (90-150°F) and (iii) no greater than 59 wt% SiO<sub>2</sub>. It has been found that a forming temperature of greater than 1240°C can accelerate the precious metal loss in the glass fiber forming bushings. In other nonlimiting embodiments of the present invention, the forming temperature is no greater than 1230°C, or no greater than 1220°C, or no greater than 1210°C, or no greater than 1200°C.

For comparison purposes, Table G also includes similar features of selected Type I-1 and I-2 glasses, two commercial boron containing E-glass compositions, and two commercial ADVANTEX glass compositions. It is noted that none of these

- 29 -

specific examples meets the selection criteria for the glasses of the present invention presented in Table G.

TABLE G

Composition	%SiO <sub>2</sub>	SiO <sub>2</sub> /RO	T <sub>FORM</sub> (°C)	T <sub>LIQ</sub> (°C)	ΔT (°C)
commercial glass 1 <sup>1</sup> (5.1 wt% B <sub>2</sub> O <sub>3</sub> )	55.2	2.31	1207	1069	138
commercial glass 2 <sup>1</sup> (6.1 wt% B <sub>2</sub> O <sub>3</sub> )	53.1	2.32	1172	1077	95
Type I-1 glass (no boron)					
from Patent '106	59	2.27	1249 <sup>2</sup>	1149	100
from Patent '144 – Ex. 1	60.18	2.46	1255 <sup>2</sup>	1180	75
from Patent '329	59.05-60.08	2.18-2.43	1248-1289 <sup>2</sup>	1169-1219	56-96
commercial ADVANTEX glass sample 1 <sup>3</sup>	59.36	2.26	1268	1180	88
commercial ADVANTEX glass sample 2 <sup>3</sup>	60.17	2.28	1266	1189	77
Type I-2 glass					
from Patent '144 – Ex. 2 (1.8 wt% B <sub>2</sub> O <sub>3</sub> )	60.82	2.53	1262 <sup>2</sup>	1180	82
Selection criteria	≤ 59		≤ 1240		50-83
Type II-1 (no boron)	57.45-58.05	2.13-2.21	1232-1240	1164-1167	66-74
Type II-2 (w/ B <sub>2</sub> O <sub>3</sub> )	55.4-58.55	2.03-2.28	1202-1240	1127-1178	55-83
Type III-1 (no boron)	57.65-58.96	2.16-2.26	1205-1237	1146-1172	52-69
Type III-2 (no boron)	57.35-58.30	2.18-2.29	1195-1213	1136-1157	54-71
Type III-3 (no boron)	58.19-59.00	2.24-2.28	1212-1234	1159-1181	50-69
Type III-4 (w/ B <sub>2</sub> O <sub>3</sub> )	57.60-58.80	2.17-2.32	1192-1227	1125-1160	50-83

<sup>1</sup> produced by PPG Industries, Inc., Pittsburgh, PA.

<sup>2</sup> glass standard unknown

<sup>3</sup> sample analyzed using X-ray fluorescence analysis

Referring to Table G, it can be seen that the selected boron-free Type II-1, III-1, III-2 and III-3 glasses generally have less SiO<sub>2</sub>, a lower SiO<sub>2</sub>/RO ratio, a lower forming temperature, and a narrower ΔT range than the sample boron-free Type I-1 glasses. Similarly, the selected boron-containing Type II-2 and III-4 glasses generally have less SiO<sub>2</sub>, a lower SiO<sub>2</sub>/RO ratio, a lower forming temperature, and a narrower ΔT range than the sample boron-containing Type I-2 glasses. Furthermore, the selected Type II and III glasses generally have a higher SiO<sub>2</sub> content, a lower SiO<sub>2</sub>/RO ratio, and a narrower ΔT range than the two commercial, high boron content samples.

- 30 -

Tables H, I, J and K illustrate additional glass compositions according to the present invention.

TABLE H

Composition Weight %	Examples										
	299	300	301	302	303	304	305	306	307	308	309
SiO <sub>2</sub>	56.25	56.45	56.75	56.50	56.75	57.5	56.75	57.75	57.75	57.75	55.40
Al <sub>2</sub> O <sub>3</sub>	13.2	13.20	13.20	13.20	13.20	12.2	13.2	12.2	12.2	12.2	13.6
CaO	24.25	24.25	23.95	24.00	23.75	24	23.95	23.75	23.75	23.95	24.5
MgO	2.55	2.55	2.55	2.55	2.55	2.55	2.55	2.55	2.55	2.55	2.95
TiO <sub>2</sub>	1.10	1.10	1.10	1.10	1.10	1.10	1.10	1.10	1.10	1.10	1.10
Na <sub>2</sub> O	0.9	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.45
K <sub>2</sub> O											0.45
Fe <sub>2</sub> O <sub>3</sub>	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25
B <sub>2</sub> O <sub>3</sub>	1.30	1.30	1.30	1.30	1.40	1.30	1.20	1.40	1.30	1.40	1.30
SiO <sub>2</sub> /RO	2.10	2.11	2.14	2.13	2.16	2.17	2.14	2.20	2.20	2.18	2.02
T <sub>FORM</sub> (°C)	1210	1214	1215	1215	1215	1216	1216	1217	1217	1218	1210
T <sub>LIQ</sub> (°C)	1154	1159	1154	1154	1160	1152	1147	1151	1147	1155	1157
ΔT (°C)	56	55	61	61	55	64	69	66	70	63	53

5

TABLE H (cont'd)

Composition Weight %	Examples										
	310	311	312	313	314	315	316	317	318	319	320
SiO <sub>2</sub>	55.40	56.05	55.85	56.00	56.60	56.50	56.10	56.50	55.95	56.50	56.45
Al <sub>2</sub> O <sub>3</sub>	13.60	13.10	13.38	13.37	13.25	13.45	13.38	13.45	13.95	13.49	13.48
CaO	24.50	24.55	24.67	24.53	24.60	24.50	24.42	24.50	24.55	24.46	24.52
MgO	2.95	2.75	2.55	2.55	2.55	2.55	2.55	2.55	2.55	2.55	2.55
TiO <sub>2</sub>	1.10	1.10	1.10	1.10	0.55	0.55	0.55	0.55	0.55	0.55	0.55
Na <sub>2</sub> O	0.45	0.45	0.45	0.45	0.90	0.90	0.90	0.90	0.90	0.90	0.90
K <sub>2</sub> O	0.45	0.45	0.45	0.45							
Fe <sub>2</sub> O <sub>3</sub>	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25
B <sub>2</sub> O <sub>3</sub>	1.30	1.30	1.30	1.30	1.30	1.30	1.30	1.30	1.30	1.30	1.30
SiO <sub>2</sub> /RO	2.02	2.05	2.05	2.07	2.09	2.09	2.08	2.09	2.07	2.09	2.09
T <sub>FORM</sub> (°C)	1211	1218	1220	1221	1211	1212	1215	1215	1216	1218	1219
T <sub>LIQ</sub> (°C)	1151	1156	1148	1157	1153	1158	1150	1157	1162	1161	1158
ΔT (°C)	60	62	72	64	58	54	65	58	54	57	61



- 31 -

TABLE I

Composition Weight %	Examples											
	312	322	323	324	325	326	327	328	329	330	331	332
SiO <sub>2</sub>	55.50	55.25	55.00	55.75	55.50	55.25	54.20	54.50	54.12	55.00	54.50	54.70
Al <sub>2</sub> O <sub>3</sub>	13.20	13.20	13.20	13.30	13.30	13.30	13.35	13.25	13.30	13.25	13.25	13.20
CaO	23.50	23.75	24.00	23.70	23.95	24.20	24.55	24.55	24.55	24.25	24.55	24.50
MgO	2.55	2.55	2.55	2.55	2.55	2.55	2.55	2.55	3.00	2.55	2.67	2.55
TiO <sub>2</sub>	1.10	1.10	1.10	0.55	0.55	0.55	0.55	0.55	0.55	0.55	0.55	0.55
Na <sub>2</sub> O	0.90	0.90	0.90	0.90	0.90	0.90	0.45	0.45	0.45	0.45	0.45	0.45
K <sub>2</sub> O							0.55	0.55	0.55	0.55	0.55	0.55
B <sub>2</sub> O <sub>3</sub>	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00
Fe <sub>2</sub> O <sub>3</sub>	0.250	0.250	0.250	0.250	0.250	0.250	0.28	0.28	0.28	0.28	0.28	0.28
F							0.20	0.20	0.10	0.10	0.10	0.10
SrO							0.12	0.12	0.10	0.12	0.10	0.12
SiO <sub>2</sub> /RO	2.13	2.10	2.07	2.12	2.09	2.07	1.99	2.01	1.96	2.05	2.00	2.02
T <sub>FORM</sub> (°C)	1193	1198	1201	1201	1200	1198	1190	1194	1196	1197	1201	1201
T <sub>LIQ</sub> (°C)	1129	1122	1127	1127	1129	1128	1120	1124	1132	1124	1131	1119
ΔT (°C)	64	76	74	74	71	70	70	70	64	73	70	82

TABLE J

Composition Weight %	Examples			
	333	334	335	336
SiO <sub>2</sub>	53.05	53.50	53.00	53.00
Al <sub>2</sub> O <sub>3</sub>	14.01	14.00	13.50	13.10
CaO	24.28	24.00	24.00	24.00
MgO	1.00	1.50	2.50	2.90
TiO <sub>2</sub>	0.52	0.50	0.50	0.50
Na <sub>2</sub> O	0.53	0.90	0.90	0.90
Fe <sub>2</sub> O <sub>3</sub>	0.91	0.10	0.10	0.10
B <sub>2</sub> O <sub>3</sub>	5.10	4.94	4.93	5.02
K <sub>2</sub> O	0.10	0.37	0.37	0.37
F	0.52	0.50	0.50	0.50
SrO	0.13	0.13	0.13	0.13
Cr <sub>2</sub> O <sub>3</sub>		0.13	0.13	0.13
SiO <sub>2</sub> /RO	2.01	2.10	2.00	1.97
T <sub>FORM</sub> (°C)	1171	1177	1172	1167
T <sub>LIQ</sub> (°C)	1114	1122	1103	1110
ΔT (°C)	57	57	69	57

TABLE K

Composition Weight %	Examples		
	337	338	339
SiO <sub>2</sub>	54.60	56.75	57.85
Al <sub>2</sub> O <sub>3</sub>	13.35	13.20	12.45
CaO	24.55	23.95	24.05
MgO	2.55	2.55	2.55
TiO <sub>2</sub>	0.35	1.10	0.55
Na <sub>2</sub> O	0.15	0.60	0.60
Fe <sub>2</sub> O <sub>3</sub>	0.28	0.25	0.35
B <sub>2</sub> O <sub>3</sub>	3.00	1.40	1.30
K <sub>2</sub> O	0.55		
F	0.20		
SrO	0.12		
Li <sub>2</sub> O	0.30	0.30	0.30
SiO <sub>2</sub> /RO	2.19	2.27	2.35
T <sub>FORM</sub> (°C)	1187	1206	1208
T <sub>LIQ</sub> (°C)	1133	1152	1154
ΔT (°C)	54	54	54

- 32 -

More particularly, the compositions in Table H are Type II-2 glass compositions, i.e. low boron content glasses having 1.2 to 1.4 wt%  $B_2O_3$ , which have a low  $SiO_2$  content ranging from 55.4 to 57.75 wt%, a  $SiO_2/RO$  ratio ranging from 2.02 to 2.20, a forming temperature ranging from 1210 to 1221°C and a  $\Delta T$  ranging from 54 to 72°C. Table I compositions are also low boron Type II-2 compositions the include 3 wt%  $B_2O_3$ . These compositions have a low  $SiO_2$  content ranging from 54.12 to 55.75 wt%, a  $SiO_2/RO$  ratio ranging from 1.96 to 2.13, a forming temperature ranging from 1193 to 1201°C and a  $\Delta T$  ranging from 64 to 82°C. Table J includes additional Type II-2 compositions having a  $B_2O_3$  of around 5 wt%. Of particular note for the compositions in Table J are the low  $SiO_2$  contents (53.00 to 53.50 wt%),  $SiO_2/RO$  ratios (1.97 to 2.10), forming temperatures (1167 to 1177°C), and  $\Delta T$  range (57 to 69°C). Table K includes Type III-4 compositions that have a low  $SiO_2$  content ranging from 54.60 to 57.85 wt%, a  $SiO_2/RO$  ratio ranging from 2.19 to 2.35, a forming temperature ranging from 1187 to 1208°C and a  $\Delta T$  of 54°C.

Based on the above, in one nonlimiting embodiment of the present invention, the glass fiber composition comprises 52 to 62 percent by weight  $SiO_2$ , 0 to 2 percent by weight  $Na_2O$ , 16 to 25 percent by weight  $CaO$ , 8 to 16 percent by weight  $Al_2O_3$ , 0.05 to 0.80 percent by weight  $Fe_2O_3$ , 0 to 2 percent by weight  $K_2O$ , 1 to 5 percent by weight  $MgO$ , 0 to 5 percent by weight  $B_2O_3$ , 0 to 2 percent by weight  $TiO_2$ , and 0 to 1 percent by weight F, wherein the glass composition has a log 3 forming temperature of no greater than 1240°C based on an NIST 714 reference standard, a  $\Delta T$  of at least 50°C, and a  $SiO_2/RO$  ratio of no greater than 2.35. In another nonlimiting embodiment, the  $SiO_2$  content of the glass composition is no greater than 59 percent by weight,  $\Delta T$  is in the range from 50 to 83°C, and the  $SiO_2/RO$  ratio is in the range from 1.9 to 2.3, and further the log 3 forming temperature is no greater than 1230°C based on an NIST 714 reference standard. In still another nonlimiting embodiment, the glass composition is boron-free.

In another nonlimiting embodiment of the present invention, the glass fiber composition comprises 53 to 59 percent by weight  $SiO_2$ , 0 to 2 percent by weight  $Na_2O$ , 16 to 25 percent by weight  $CaO$ , 8 to 16 percent by weight  $Al_2O_3$ , 0.05 to 0.80 percent by weight  $Fe_2O_3$ , 0 to 2 percent by weight  $K_2O$ , 1 to 4 percent by weight  $MgO$ , 0 to 5 percent by weight  $B_2O_3$ , 0 to 2 percent by weight  $TiO_2$ , and 0 to 1 percent by weight F, wherein the glass composition has a log 3 forming temperature

- 33 -

of no greater than 1240°C based on an NIST 714 reference standard, a  $\Delta T$  in the range of 50 to 100°C, and a  $\text{SiO}_2/\text{RO}$  ratio in the range of 1.9 to 2.3.

In viewing the tables and figures, it should be appreciated that many of the sample compositions, although they have a  $\Delta T$  greater than the minimum required

5  $\Delta T$  for a particular process, they also have a higher forming temperature than that of the compositions of the present invention due, in part, to their high silica levels and/or high  $\text{SiO}_2/\text{RO}$  ratios. As a result, such compositions are more expensive to produce commercially, at least in terms of energy costs. Such compositions include the Type I compositions discussed herein. In addition, the tables and figures contain

10 many samples containing a  $\Delta T$  less than the minimum desired  $\Delta T$  of 50°C (90°F). These types of compositions can be found across the compositional spectrum in each figure but especially at low silica and  $\text{SiO}_2/\text{RO}$  levels. Because of the narrower  $\Delta T$  range, the risk of the molten glass solidifying in the bushing area during a glass fiber forming operation increases to an unacceptable level.

15 It will be appreciated by those skilled in the art that changes could be made to the embodiments described above without departing from the broad inventive concept thereof. It is understood, therefore, that this invention is not limited to the particular embodiments disclosed, but it is intended to cover modifications that are within the spirit and scope of the invention, as defined by the appended claims.

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- 34 -

## I CLAIM:

1. A glass fiber composition comprising:

SiO <sub>2</sub>	52 to 62 percent by weight;
Na <sub>2</sub> O	0 to 2 percent by weight;
CaO	16 to 25 percent by weight;
Al <sub>2</sub> O <sub>3</sub>	8 to 16 percent by weight;
Fe <sub>2</sub> O <sub>3</sub>	0.05 to 0.80 percent by weight;
K <sub>2</sub> O	0 to 2 percent by weight;
MgO	1 to 5 percent by weight;
B <sub>2</sub> O <sub>3</sub>	0 to 5 percent by weight;
TiO <sub>2</sub>	0 to 2 percent by weight; and
F	0 to 1 percent by weight;

- 5 wherein the glass composition has a log 3 forming temperature of no greater than 1240°C based on an NIST 714 reference standard, a  $\Delta T$  of at least 50°C, and a SiO<sub>2</sub>/RO ratio of no greater than 2.35.

2. The glass fiber composition according to claim 1, wherein the SiO<sub>2</sub> content is no greater than 59 percent by weight,  $\Delta T$  is in the range from 50 to 83°C, and the SiO<sub>2</sub>/RO ratio is in the range from 1.9 to 2.3.

3. The glass fiber composition according to claim 2, wherein the SiO<sub>2</sub> content is no greater than 58 percent by weight.

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4. The glass fiber composition according to claim 2, wherein the log 3 forming temperature is no greater than 1230°C based on an NIST 714 reference standard.

- 20 5. The glass fiber composition according to claim 4, wherein the log 3 forming temperature is no greater than 1210°C based on an NIST 714 reference standard.

- 25 6. The glass fiber composition according to claim 2, wherein the B<sub>2</sub>O<sub>3</sub> content is no greater than 3 percent by weight.

- 35 -

7. The glass fiber composition according to claim 6, wherein the  $B_2O_3$  content is no greater than 2 percent by weight.

5 8. The glass fiber composition according to claim 2, wherein the glass composition is boron-free.

9. The glass fiber composition according to claim 2, wherein the  $SiO_2/RO$  ratio is no greater than 2.25.

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10. The glass fiber composition according to claim 9, wherein the  $SiO_2/RO$  ratio is no greater than 2.20.

11. The glass fiber composition according to claim 2, wherein the MgO content is 1.7 to 2.9 percent by weight, the  $B_2O_3$  content is no greater than 3 percent by weight, and the  $TiO_2$  content is no greater than 1.5 percent by weight.

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12. The glass fiber composition according to claim 11, wherein the glass composition is boron-free.

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13. The glass fiber composition according to claim 2, wherein the glass composition further includes at least one material selected from:

$Li_2O$	0.05 to 1.5 percent by weight;
$ZnO$	0.05 to 1.5 percent by weight;
$MnO$	0.05 to 3 percent by weight; and
$MnO_2$	0.05 to 3 percent by weight.

14. The glass fiber composition according to claim 1, wherein the MgO content is 1 to 4 percent by weight, the  $B_2O_3$  content is no greater than 4 percent by weight, and the  $TiO_2$  content is no greater than 2 percent by weight.

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15. The glass fiber composition according to claim 14, wherein the forming temperature is no greater than 1230°C based on an NIST 714 reference standard.

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- 36 -

16. The glass fiber composition according to claim 14, wherein the  $\text{SiO}_2/\text{RO}$  ratio is no greater than 2.30.

5 17. The glass fiber composition according to claim 14, wherein  $\Delta T$  is in the range from 50 to 83°C.

18. The glass fiber composition according to claim 1, wherein the forming temperature is no greater than 1230°C based on an NIST 714 reference standard.

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19. The glass fiber composition according to claim 18, wherein the forming temperature is no greater than 1220°C based on an NIST 714 reference standard.

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20. The glass fiber composition according to claim 19, wherein the forming temperature is no greater than 1210°C based on an NIST 714 reference standard.

21. The glass fiber composition according to claim 1, wherein the  $\text{SiO}_2$  content is no greater than 59 percent by weight.

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22. The glass fiber composition according to claim 21, wherein the  $\text{SiO}_2$  content is no greater than 58 percent by weight.

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23. The glass fiber composition according to claim 1, wherein the  $\text{TiO}_2$  content is no greater than 1.5 percent by weight.

24. The glass fiber composition according to claim 1, wherein the  $\text{MgO}$  content is 1 to 4 percent by weight

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25. The glass fiber composition according to claim 24, wherein the  $\text{MgO}$  content is 1.9 to 2.65 percent by weight

- 37 -

26. The glass fiber composition according to claim 1, wherein the  $B_2O_3$  content is no greater than 4 percent by weight.

27. The glass fiber composition according to claim 26, wherein the  $B_2O_3$  content is no greater than 2 percent by weight.

28. The glass fiber composition according to claim 1, wherein the glass composition is boron-free.

29. The glass fiber composition according to claim 1, wherein the glass composition is fluorine-free.

30. The glass fiber composition according to claim 1, wherein the  $SiO_2/RO$  ratio is no greater than 2.30.

31. The glass fiber composition according to claim 31, wherein the  $SiO_2/RO$  ratio is no greater than 2.25.

32. The glass fiber composition according to claim 32, wherein the  $SiO_2/RO$  ratio is no greater than 2.20.

33. The glass fiber composition according to claim 1, wherein the  $SiO_2/RO$  ratio is in the ranges from 1.9 to 2.30.

34. The glass fiber composition according to claim 33, wherein the  $SiO_2/RO$  ratio is in the ranges from 2.05 to 2.29.

35. The glass fiber composition according to claim 1, wherein  $\Delta T$  is at least  $55^\circ C$ .

36. The glass fiber composition according to claim 1, wherein  $\Delta T$  is in the range from  $50$  to  $100^\circ C$ .

- 38 -

37. The glass fiber composition according to claim 36, wherein  $\Delta T$  is in the range from 50 to 83°C.

38. The glass fiber composition according to claim 1, wherein the glass composition further includes at least one material selected from:

Li <sub>2</sub> O	0.05 to 1.5 percent by weight;
ZnO	0.05 to 1.5 percent by weight;
MnO	0.05 to 3 percent by weight; and
MnO <sub>2</sub>	0.05 to 3 percent by weight.

39. A glass fiber composition comprising:

SiO <sub>2</sub>	53 to 59 percent by weight;
Na <sub>2</sub> O	0 to 2 percent by weight;
CaO	16 to 25 percent by weight;
Al <sub>2</sub> O <sub>3</sub>	8 to 16 percent by weight;
Fe <sub>2</sub> O <sub>3</sub>	0.05 to 0.80 percent by weight;
K <sub>2</sub> O	0 to 2 percent by weight;
MgO	1 to 4 percent by weight;
B <sub>2</sub> O <sub>3</sub>	0 to 5 percent by weight;
TiO <sub>2</sub>	0 to 2 percent by weight; and
F	0 to 1 percent by weight;
Li <sub>2</sub> O	0 to 1.5 percent by weight;
ZnO	0 to 1.5 percent by weight;
MnO	0 to 3 percent by weight; and
MnO <sub>2</sub>	0 to 3 percent by weight.

wherein the glass composition has a log 3 forming temperature of no greater than 1240°C based on an NIST 714 reference standard, a  $\Delta T$  in the range from 50 to 100°C, and a SiO<sub>2</sub>/RO ratio is in the range from 1.9 to 2.30.

40. The glass fiber composition according to claim 39, wherein the glass composition has a  $\Delta T$  in the range from 50 to 83°C.

41. The glass fiber composition according to claim 39, wherein SiO<sub>2</sub>/RO ratio is no greater than 2.25.



- 39 -

42. The glass fiber composition according to claim 39, wherein the log 3 forming temperature is no greater than 1230°C based on an NIST 714 reference standard.

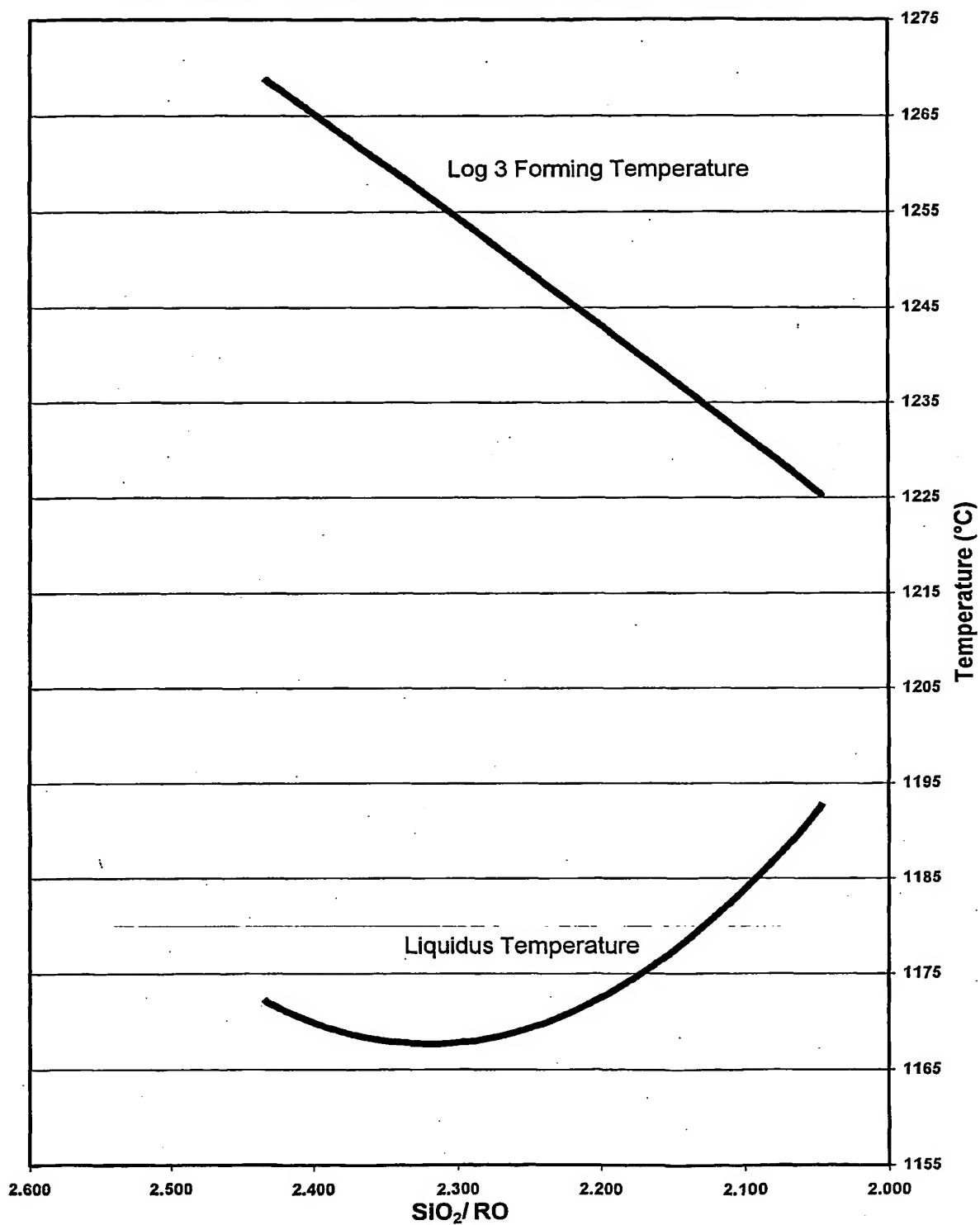
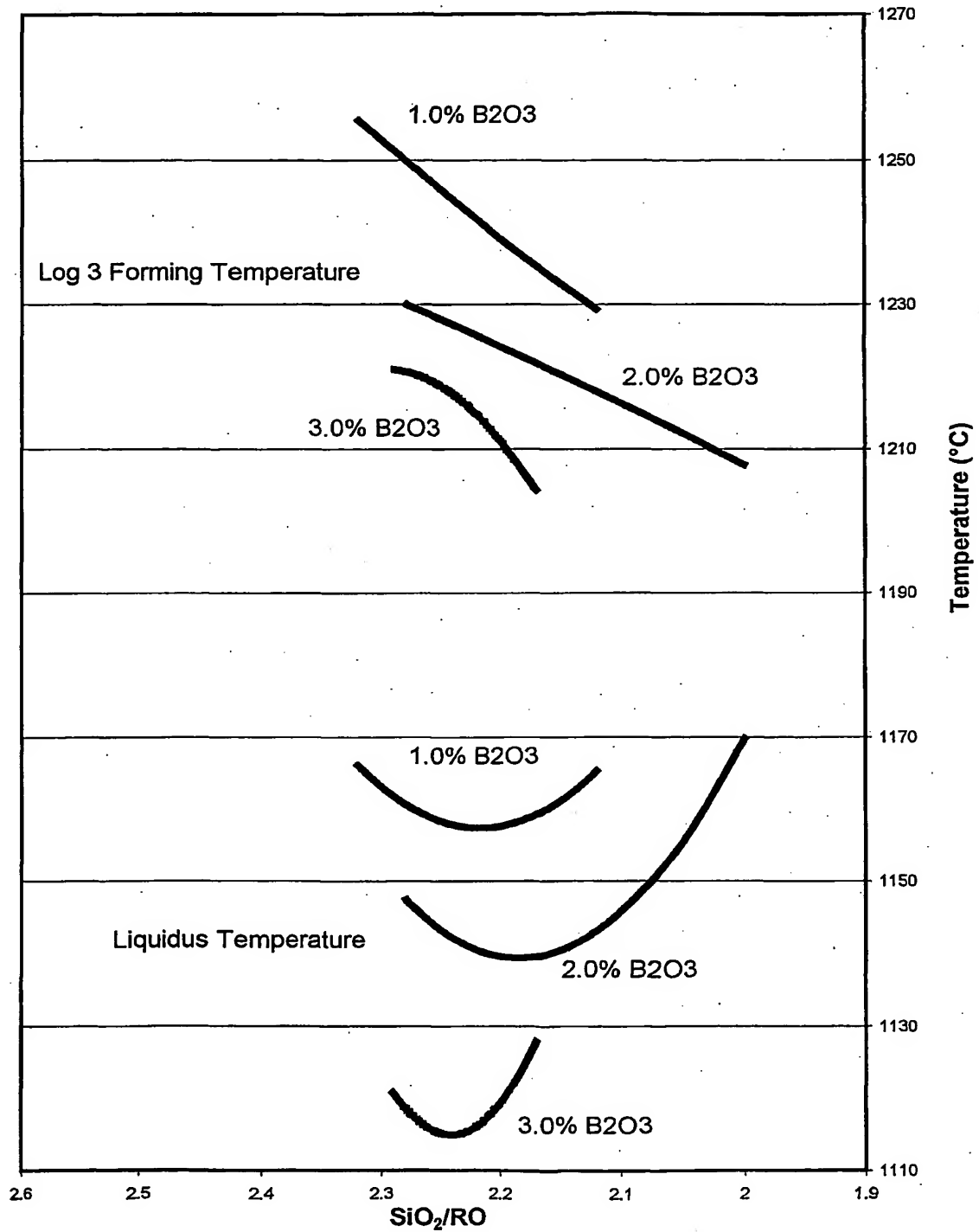
TYPE I-1/II-1 Trendlines: SiO<sub>2</sub>/RO vs. Melt Properties

FIGURE 1

**TYPE II-1/II-2 Trendlines: SiO<sub>2</sub>/RO vs. Melt Properties****FIGURE 2**

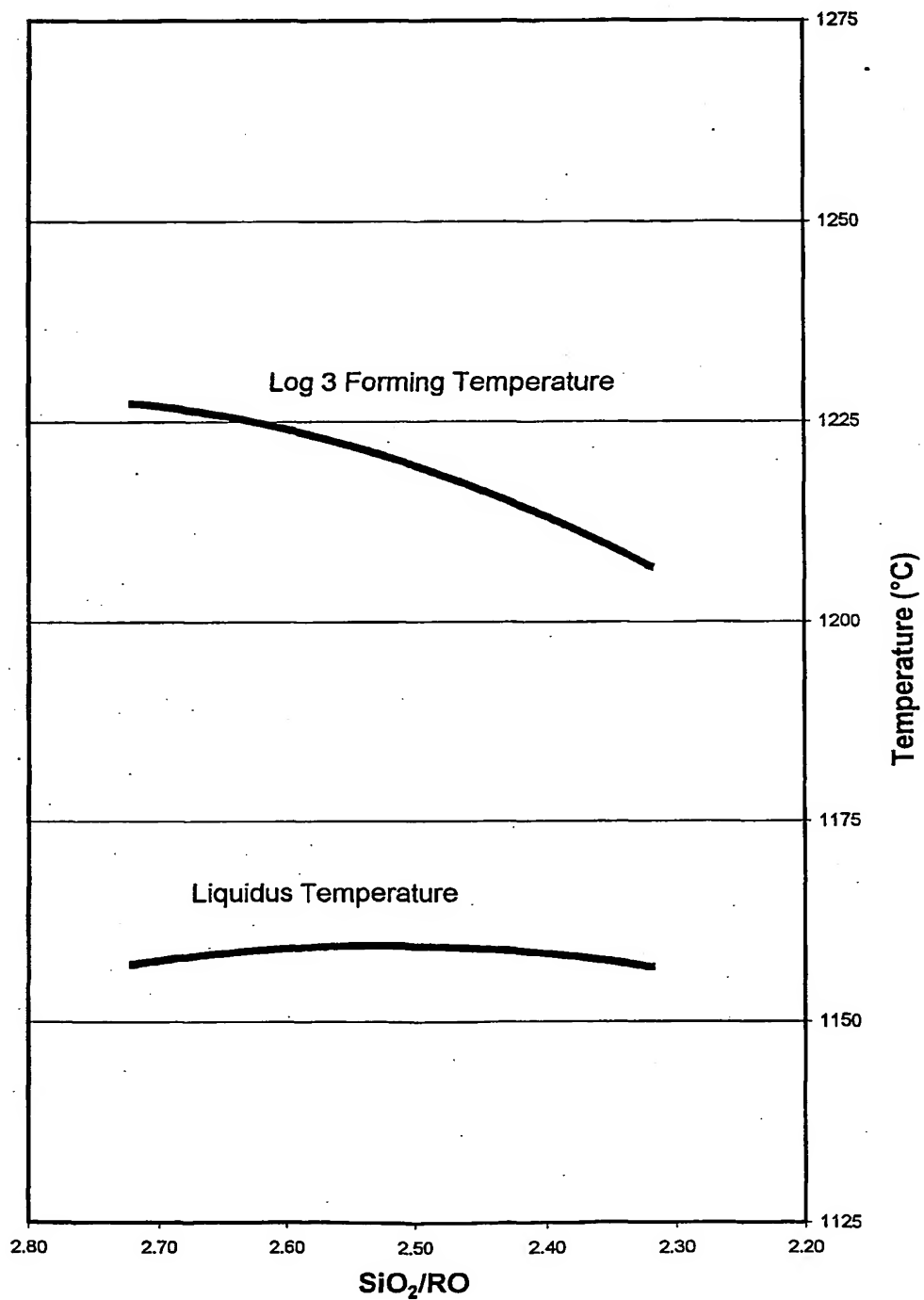
TYPE III-1 Trendlines: SiO<sub>2</sub>/RO vs. Melt Properties

FIGURE 3

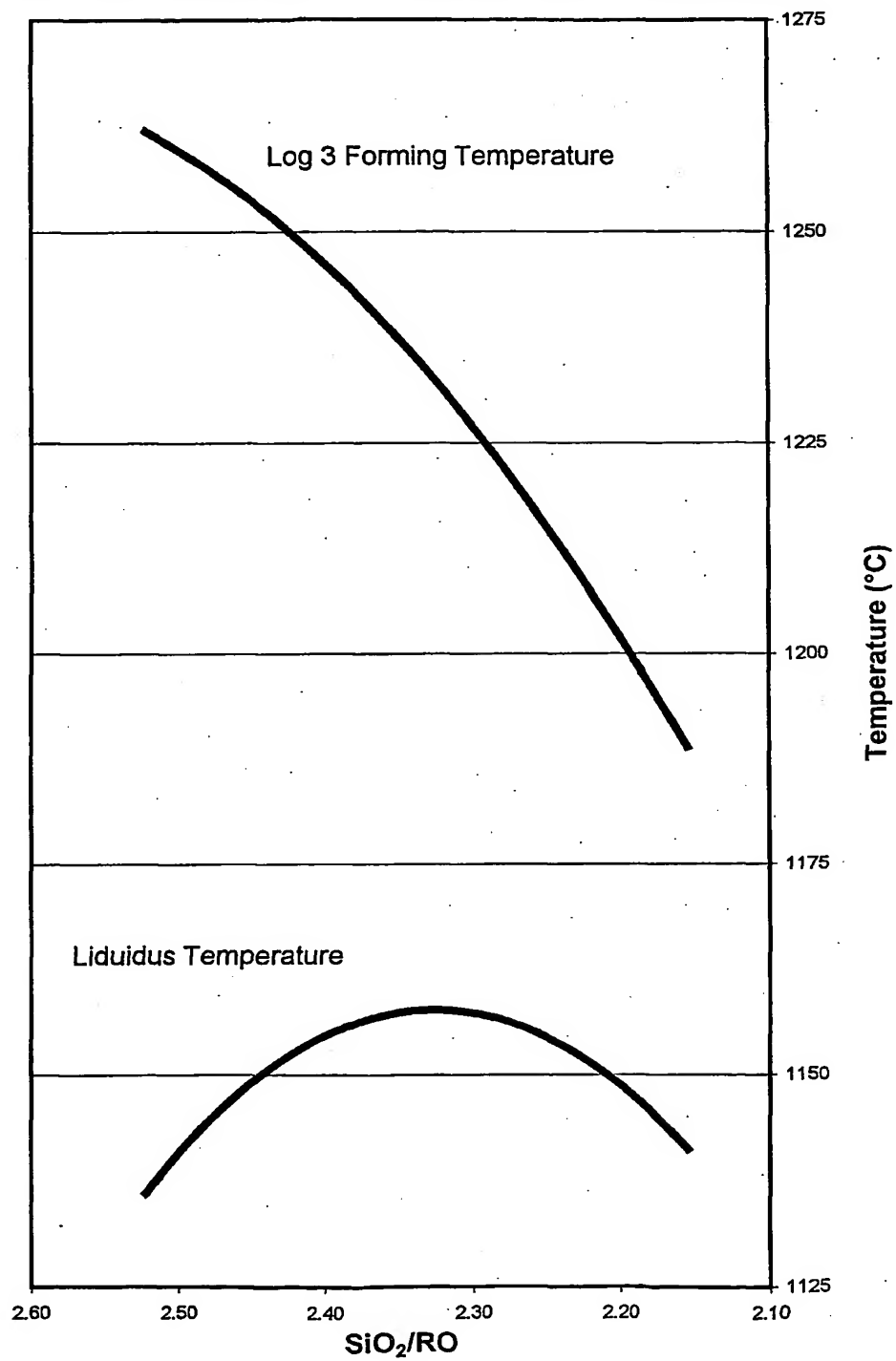
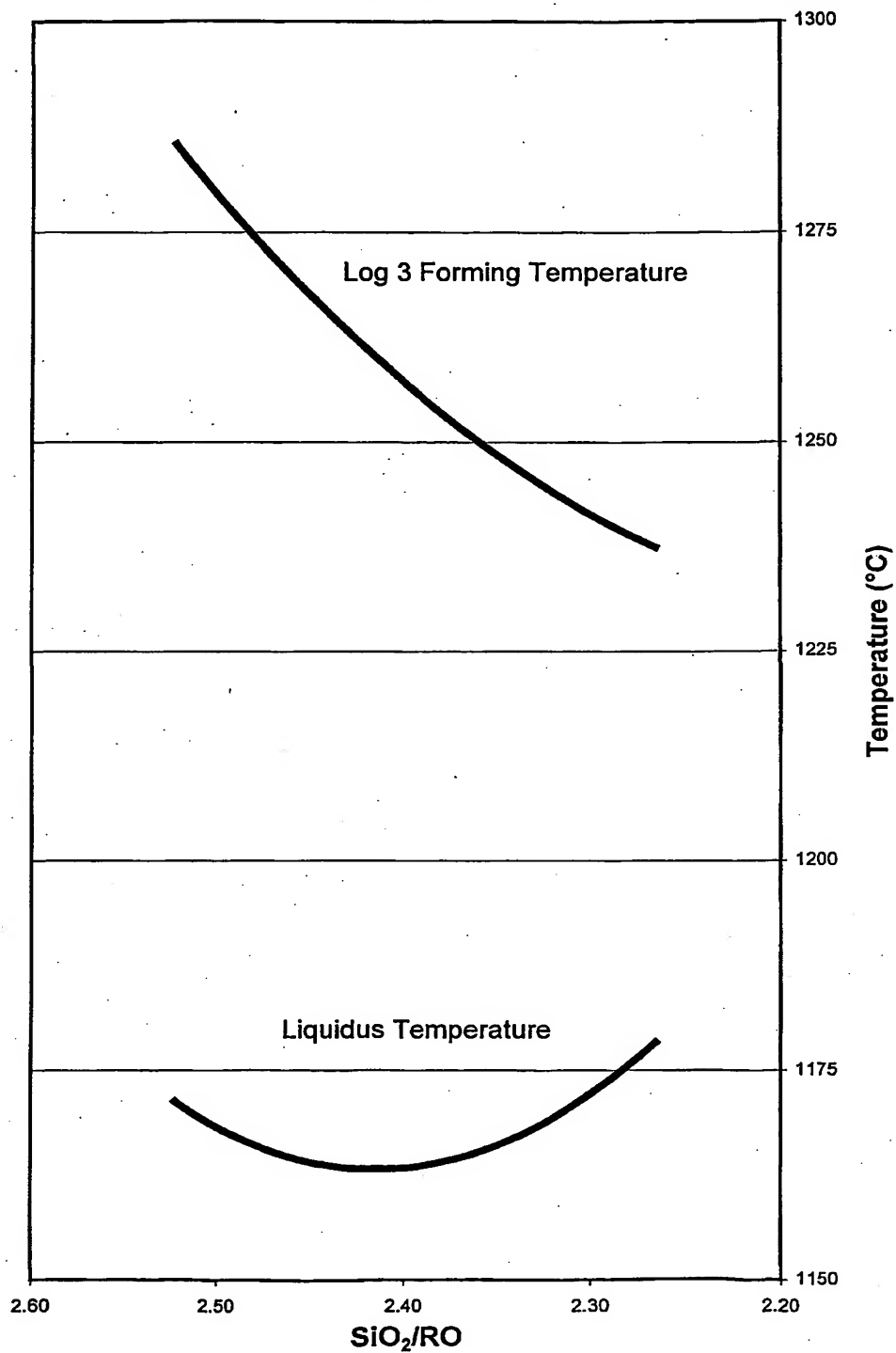
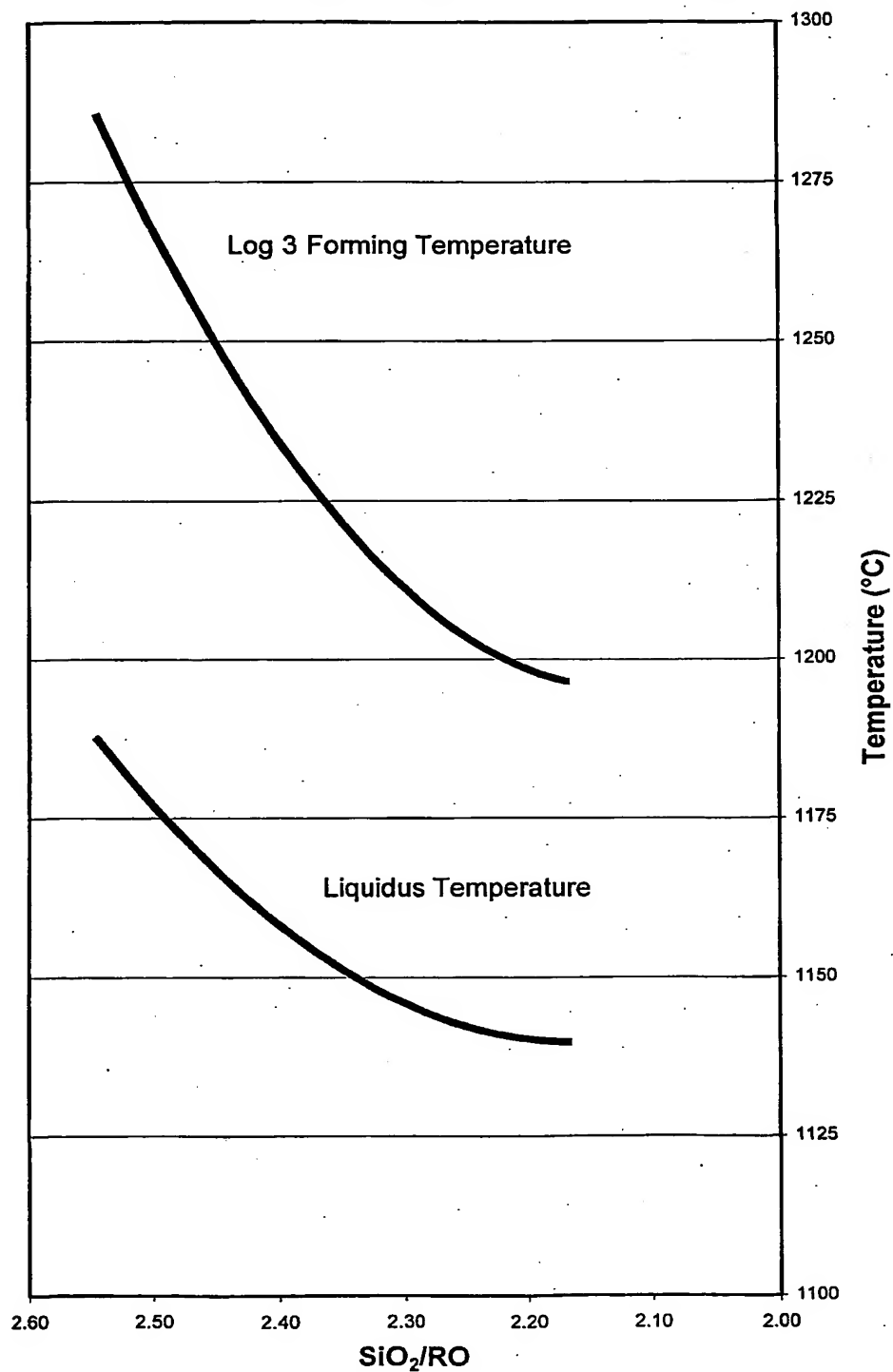
TYPE III-2 Trendlines: SiO<sub>2</sub>/RO vs. Melt Properties

FIGURE 4

**TYPE III-3 Trendlines: SiO<sub>2</sub>/RO vs. Melt Properties****FIGURE 5**

**TYPE III-4 Trendlines: SiO<sub>2</sub>/RO vs. Melt Properties****FIGURE 6**

## INTERNATIONAL SEARCH REPORT

International application No.

PCT/US01/27451

**A. CLASSIFICATION OF SUBJECT MATTER**

IPC(7) : C05C 13/06, 3/087

US CL : 501/85, 86, 70

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 501/85, 86, 70

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X, P	US 6,136,735 A (GALLO et al) 24 October 2000, col. 2, lines 5-60.	1-42
X	US 5,789,329 A (EASTES et al) 04 August 1998, col. 3, lines 1-52.	1-12, 14-37, 39-42
A	US 5,962,354 A (FYLES et al) 05 October 1999, col. 3, lines 4-30.	1-42
A	US 4,199,364 A (NEELY) 22 April 1980, col. 3, lines 40-63.	1-42
A	US 4,628,038 A (WEIRAUCH, Jr.) 09 December 1986, col. 2, lines 13-25.	1-42

☐ Further documents are listed in the continuation of Box C.
 ☐ See patent family annex.

* Special categories of cited documents:	"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
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"P" document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search 19 NOVEMBER 2001	Date of mailing of the international search report 02 JAN 2002
Name and mailing address of the ISA/US Commissioner of Patents and Trademarks Box PCT Washington, D.C. 20231 Facsimile No. (703) 805-3230	Authorized officer KARL GROUP Telephone No. (703) 805-0661 Jean Proctor Patent Specialist